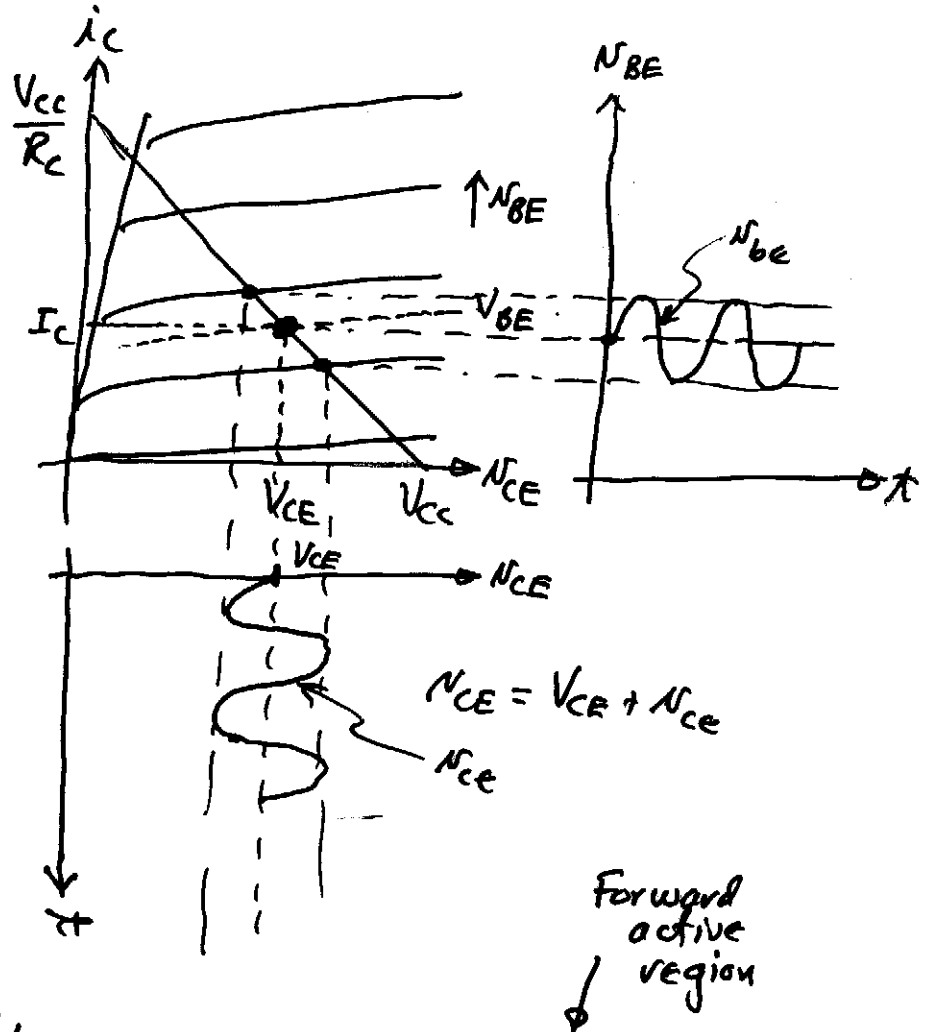
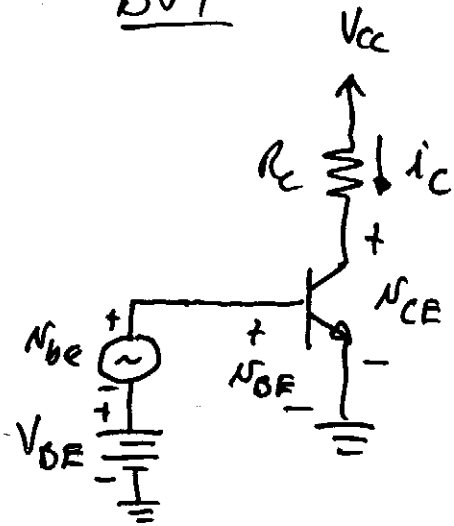


Transistor Amplifiers

BJT



Mathematically,

$$N_{CE} = V_{CC} - R_c i_c = V_{CC} - R_c \left[ I_S \exp\left(\frac{N_{BE}}{V_T}\right) \right]$$

$$\left. \frac{\partial N_{CE}}{\partial N_{BE}} \right|_{\substack{N_{BE} = V_{BE} \\ i_c = I_C}} = - \frac{R_c I_S}{V_T} \exp\left(\frac{N_{BE}}{V_T}\right) = - \frac{R_c I_S}{V_T} \exp\left(\frac{V_{BE}}{V_T}\right) = - \frac{R_c I_C}{V_T}$$

~~0.400~~

$$10^{-4} \cdot 400 = 0.04$$

$$= - \frac{R_c I_C}{V_T} = - \frac{10 \cdot 10^{-3}}{25 \cdot 10^{-3}} = -400$$

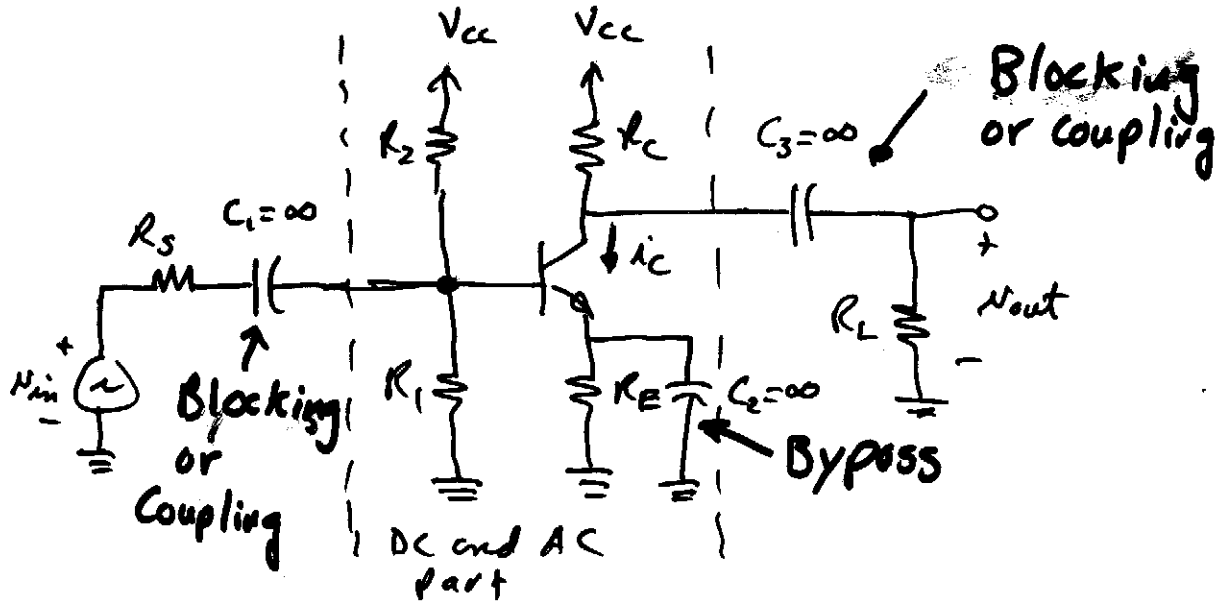
$$R_c = 10 \text{ k}\Omega$$

$$I_C = 1 \text{ mA}$$

$$V_T = 25 \text{ mV}$$

$$\text{Gain} = \frac{\partial N_{CE}}{\partial N_{BE}} = - \frac{R_c I_C}{V_T} = - \frac{10 \cdot 10^{-3}}{25 \cdot 10^{-3}} = - \frac{10,000}{25} = -400 \text{ V/V}$$

2.) Implementation of the amplifier.



3.) Small-signal model for a diode.

$$i_D = I_S \left[ \exp\left(\frac{v_D}{V_T}\right) - 1 \right]$$

$$i_d + I_D = I_S \left[ \exp\left(\frac{v_D + V_D}{V_T}\right) - 1 \right] = I_S \left[ \exp\left(\frac{v_D}{V_T}\right) \exp\left(\frac{V_D}{V_T}\right) - 1 \right]$$

Perform a series expansion, we get

$$i_d + I_D = I_S \left\{ \left[ \exp\left(\frac{V_D}{V_T}\right) \right] \left[ 1 + \frac{v_D}{V_T} + \frac{1}{2} \left(\frac{v_D}{V_T}\right)^2 + \dots \right] - 1 \right\}$$

Assume  $\frac{v_D}{V_T} \ll 1$ ,

$$\begin{aligned} i_d + I_D &\approx I_S \exp\left(\frac{V_D}{V_T}\right) \left[ 1 + \frac{v_D}{V_T} \right] - I_S \\ &= I_S \left[ \exp\left(\frac{V_D}{V_T}\right) - 1 \right] + \left[ I_S \exp\left(\frac{V_D}{V_T}\right) \right] \frac{v_D}{V_T} \end{aligned}$$

$$i_d + I_D = I_D + \left[ I_S \exp\left(\frac{V_D}{V_T}\right) \right] \frac{v_D}{V_T}$$

$$i_d = \left[ I_S \exp\left(\frac{V_D}{V_T}\right) \right] \frac{v_D}{V_T}$$

Cont'd -

$$I_D = I_S \left[ \exp\left(\frac{V_D}{V_T}\right) - 1 \right] \rightarrow I_S \exp\left(\frac{V_D}{V_T}\right) = I_D + I_S$$

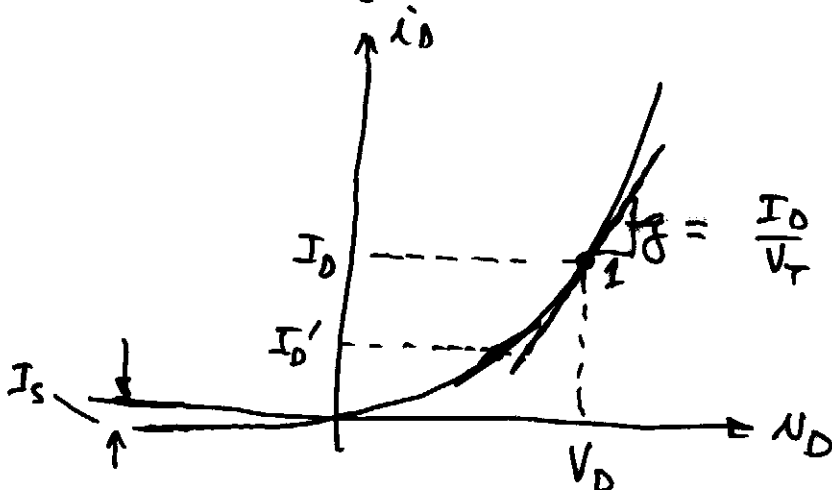
$$i_d = (I_D + I_S) \frac{v_d}{V_T} = g_d v_d = \frac{v_d}{r_d}$$

$$\underline{g_d = \frac{I_D + I_S}{V_T}} \quad \text{or} \quad \underline{r_d = \frac{1}{g_d}}$$

Normally,  $I_D \gg I_S$

$$g_d = \frac{I_D}{V_T}$$

Graphically -



Assume  $I_S = 100 \text{ fA}$

$$I_D = 1 \text{ mA} \rightarrow g_d = 0.045 \text{ S}$$

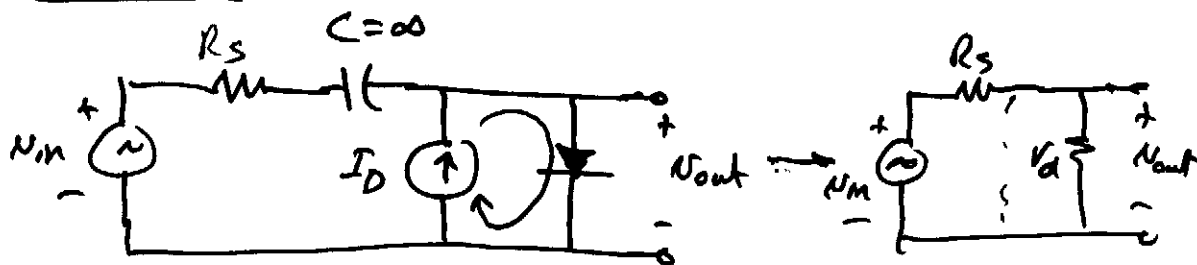
$$I_D = 0 \rightarrow g_d = \frac{100 \text{ fA}}{25 \text{ mV}}$$

$$g_d = 4 \times 10^{-12} \text{ S}$$

$$I_D = -I_S$$

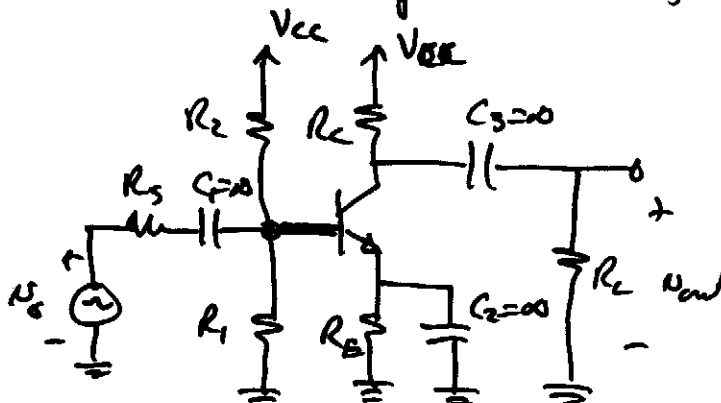
$$g_d = \frac{-I_S + I_S}{V_T} = 0$$

Homwk P1

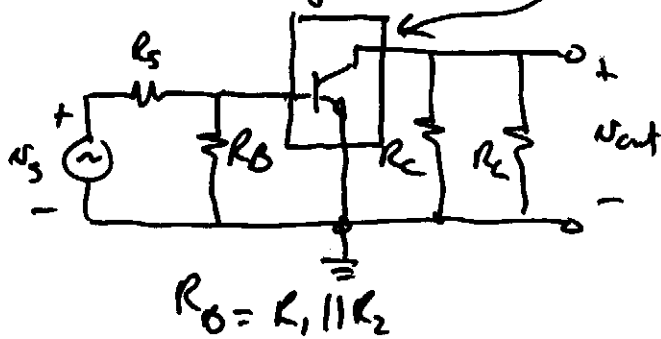


$$\frac{v_{out}}{v_{in}} = \frac{v_d}{v_d + R_s} = \frac{1}{1 + \frac{R_s}{r_d}} = \frac{1}{1 + g_d R_s} = \frac{1}{1 + R_s \left[ \frac{I_D + I_S}{V_T} \right]}$$

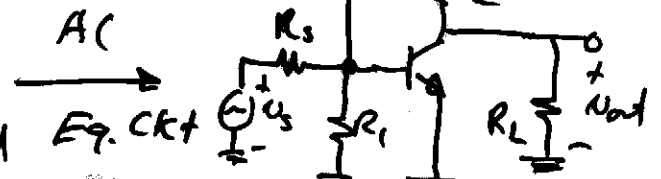
4.) Small signal model for BJT



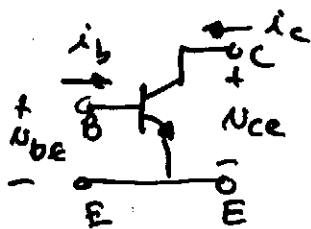
Small-signal model



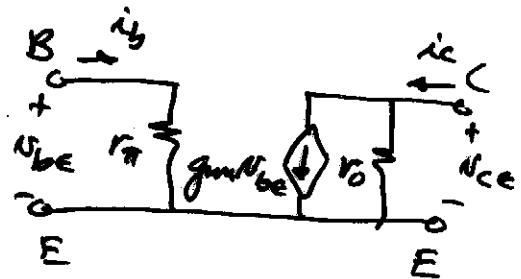
$$R_B = R_1 || R_2$$



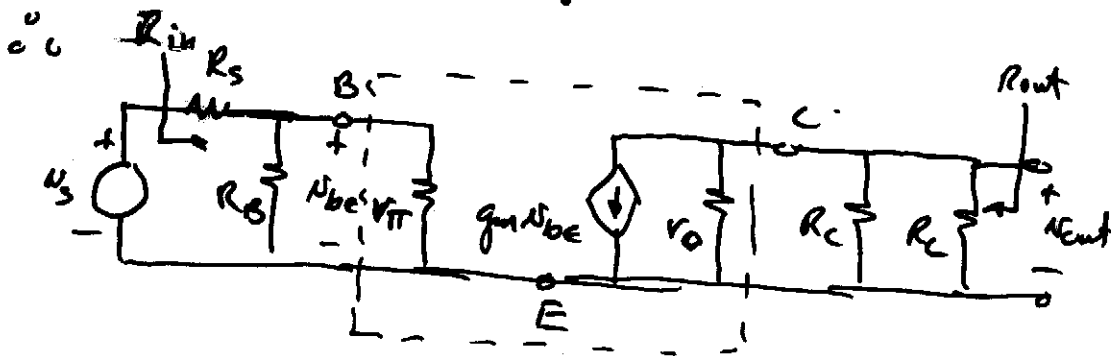
- 1.) Short caps
- 2.) Replace indep. sources with appropriate R.



Small-signal model



Remember that  $r_{\pi}$ ,  $g_m$ , and  $r_o$  are functions of  $I_c$ .



Goal is: Find  $\frac{v_{out}}{v_s}$ ,  $R_{in}$  and  $R_{out}$   
 If  $R_s = 0$

$$\frac{v_{out}}{v_s} = -g_m (r_o || R_C || R_L)$$

$$R_{in} = R_s + r_{\pi} || R_B$$

$$R_{out} = r_o || R_C || R_L$$