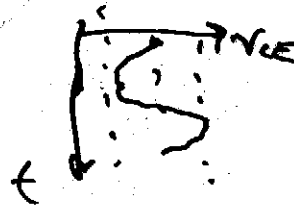
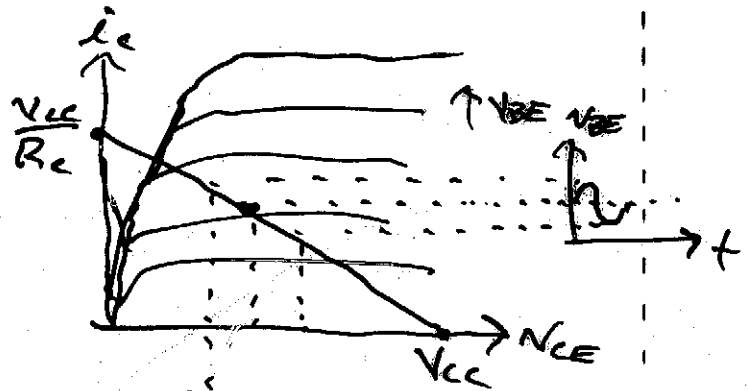
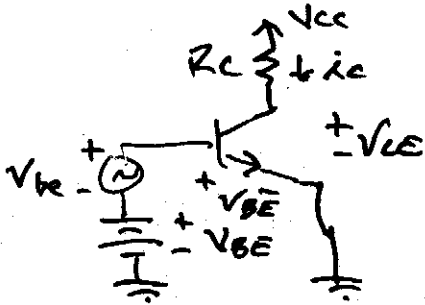


TRANSISTOR AMPLIFIERS

1.) BJT Amp

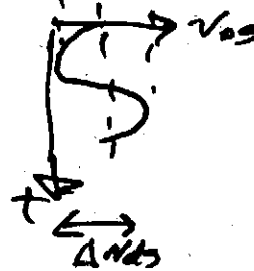
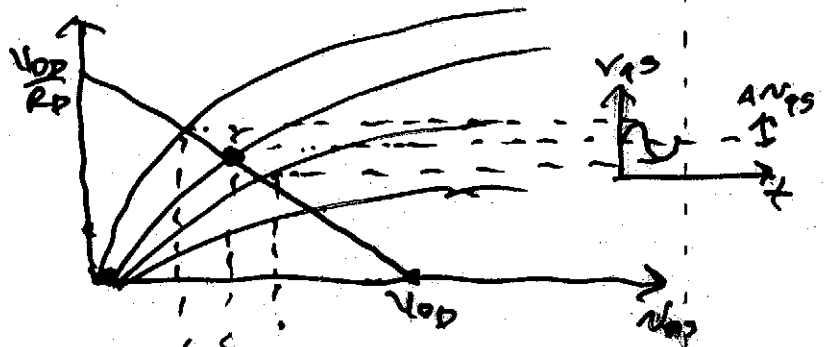
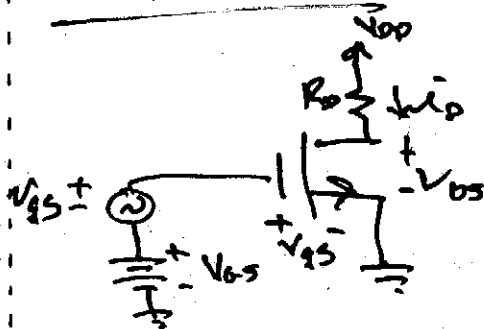


$$A_{mid} = \frac{\Delta V_{CE}}{\Delta V_{BE}}$$

$$V_{CE} = V_{CC} - i_c R_C = V_{CC} - R_C I_S \exp\left(\frac{V_{BE}}{V_T}\right)$$

$$\frac{dV_{CE}}{dV_{BE}} = -\frac{R_C I_S}{V_T} \exp\left(\frac{V_{BE}}{V_T}\right) = -\frac{R_C}{V_T} I_C \approx \frac{-10K}{25mV} \cdot 1mA = -400 \frac{V}{V}$$

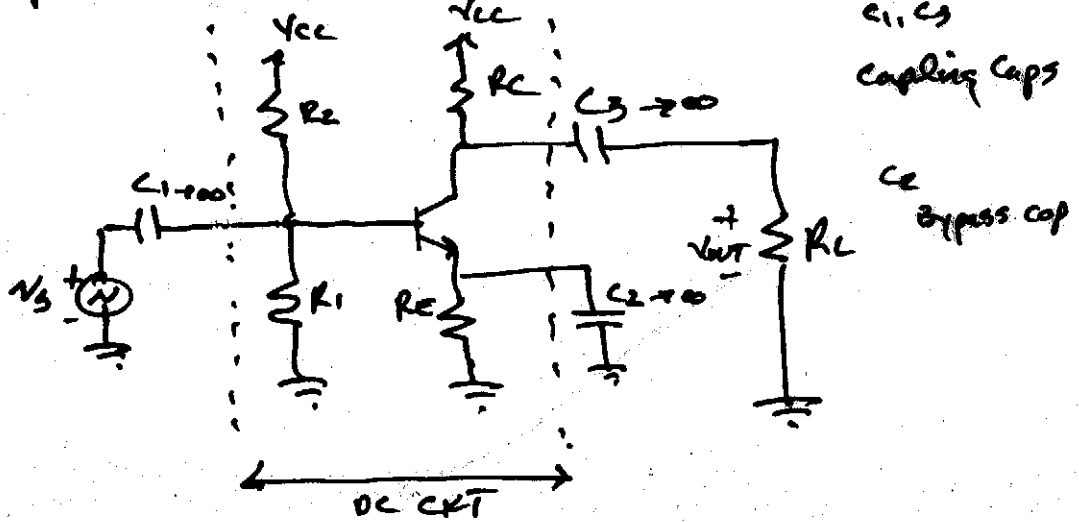
MOSFET AMPS



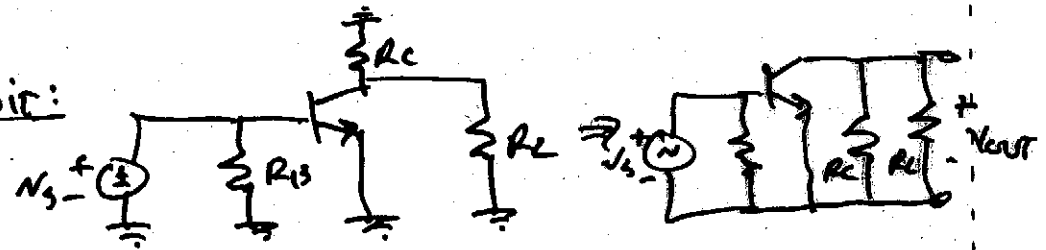
$$V_{DS} = V_{DD} - I_D R_D = V_{DD} - R_D \frac{K_n}{2} (V_{GS} - V_T)^2$$

$$\begin{aligned} \frac{dV_{DS}}{dV_{GS}} &= -R_D K_n (V_{GS} - V_T) = -R_D K_n \sqrt{\frac{2I_D}{K_n}} \\ &= -R_D \sqrt{2K_n I_D} \\ &= -10K \sqrt{2 \cdot 290 \cdot 1mA} \\ &= -7.07 \frac{V}{V} \end{aligned}$$

3.) Coupling and Bypass Capacitors



Ac circuit:



4.) Diode Small-signal model

Large signal $i_D = I_S \left[\exp\left(\frac{V_D}{V_T}\right) - 1 \right]$

$$i_d + I_D = I_S \left[\exp\left(\frac{V_D + v_d}{V_T}\right) - 1 \right] = I_S \left[\exp\left(\frac{V_D}{V_T}\right) \exp\left(\frac{v_d}{V_T}\right) - 1 \right]$$

expand $\frac{v_d}{V_T}$ by a Maclaurin series

$$i_d + I_D = I_S \left\{ \left[\exp\left(\frac{V_D}{V_T}\right) \right] \left[1 + \frac{v_d}{V_T} + \frac{1}{2} \left(\frac{v_d}{V_T}\right)^2 + \dots \right] - 1 \right\} \rightarrow I_D$$

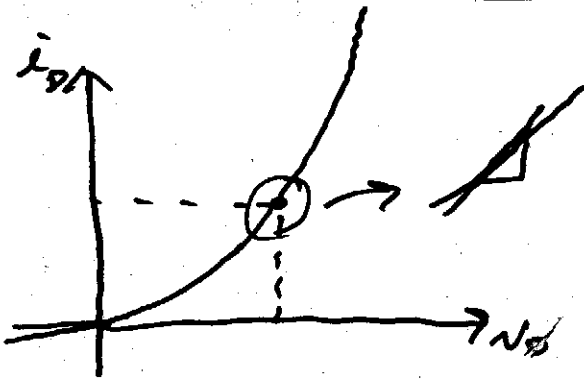
$$i_d + I_D \approx I_S \left[\exp\left(\frac{V_D}{V_T}\right) \right] \left[1 + \frac{v_d}{V_T} \right] - I_S = I_S \left[\exp\left(\frac{V_D}{V_T}\right) - 1 \right] + \left[I_S \exp\left(\frac{V_D}{V_T}\right) \right] \left(\frac{v_d}{V_T}\right)$$

$$i_d + I_D = I_D + \left[I_S \exp\left(\frac{V_D}{V_T}\right) \right] \left(\frac{v_d}{V_T}\right)$$

$$\rightarrow i_d = \frac{(I_D + I_S) v_d}{V_T} = \underline{g_m v_d}$$

$$\therefore g_m = \frac{I_D + I_S}{V_T} \approx \frac{I_D}{V_T}$$

Diode small signal model (cont.)



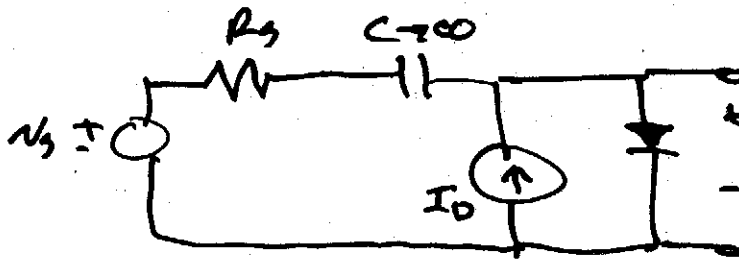
$I_D = 100 \text{ fA}$

$I_D = 1 \text{ mA} \rightarrow g_m = \frac{1 \text{ mA}}{25 \text{ mV}} = 0.04 \text{ S}$

$I_D = 0 \rightarrow g_m = \frac{100 \text{ fA}}{25 \text{ mV}} = 4 \times 10^{-12} \text{ S}$

$I_D = I_S \rightarrow g_m = 0$

Example current controlled small-signal attenuator



$$v_{out} = \frac{\frac{I_D}{g_m}}{\frac{1}{g_m} + R_s} v_s$$

$$= \frac{1}{1 + g_m R_s} v_s$$

$$v_{out} = \frac{1}{1 + \frac{I_D R_s}{V_T}} v_s$$

