

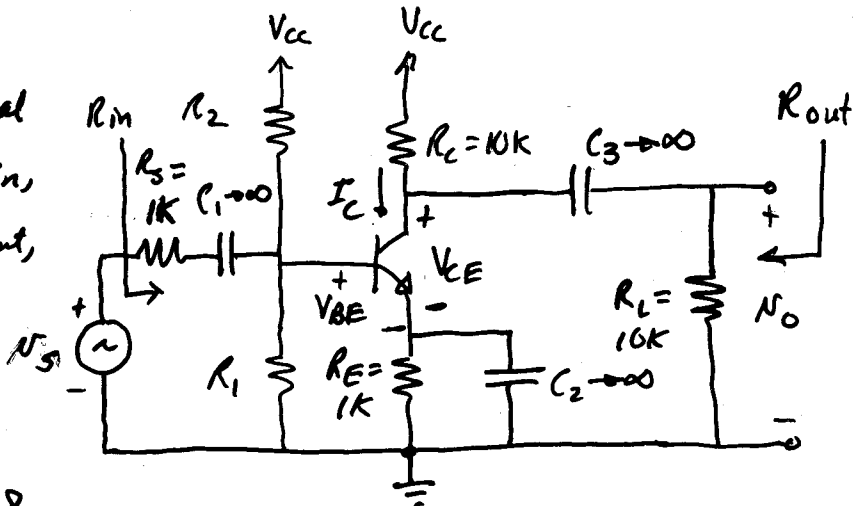
BJT Example

Find the small-signal input resistance, R_{in} , output resistance, R_{out} , and $\frac{N_o}{N_s}$ when

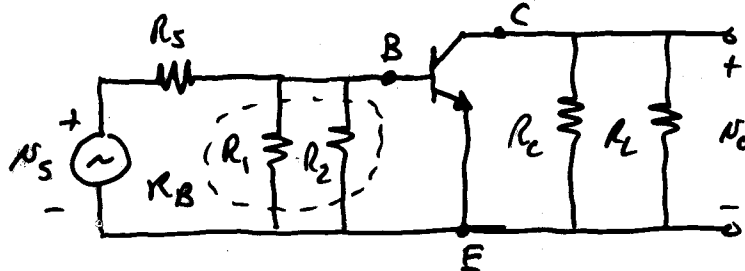
$I_C = 1mA$, $\beta_o = 100$,

$V_A = 100V$ and

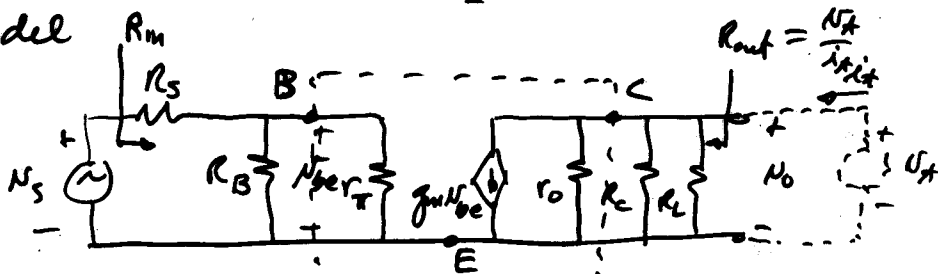
$R_B = R_1 || R_2 = 20k\Omega$



1.) Quasi-AC model ($V_{cc} = 0$ & C 's replaced by shorts)



2.) AC-Model



4.) Perform the analysis -

$R_{in}, R_{out}, \frac{N_o}{N_s}$

$R_{in} = R_s + R_B || r_{\pi} = 1k + 20k || 25k\Omega$

$R_{in} = 3.22k\Omega$

$\frac{N_o}{N_s} = \left(\frac{N_o}{N_{be}}\right) \left(\frac{N_{be}}{N_s}\right)$

3.) Find g_m, r_{π} & r_o

$g_m = \frac{I_C}{V_T} = \frac{1mA}{25mV} = 40mS$

$r_{\pi} = \frac{\beta_o}{g_m} = 25 \cdot 100 = 2.5k\Omega$

$r_o = \frac{I_C}{V_A + V_{CE}} \approx \frac{I_C}{V_A} = \frac{1mA}{100V} = 1/100k$

$r_o = 100k\Omega$

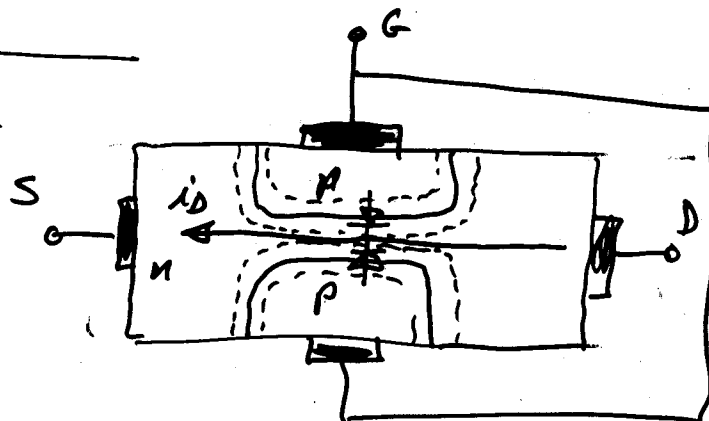
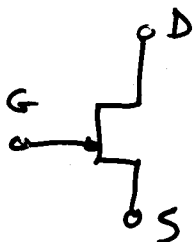
4.) Cont'd

$$\frac{V_o}{V_{be}} = -g_m (r_o \parallel R_c \parallel R_L), \quad \frac{V_{be}}{V_s} = \frac{R_B \parallel r_{\pi}}{R_s + R_B \parallel r_{\pi}}$$

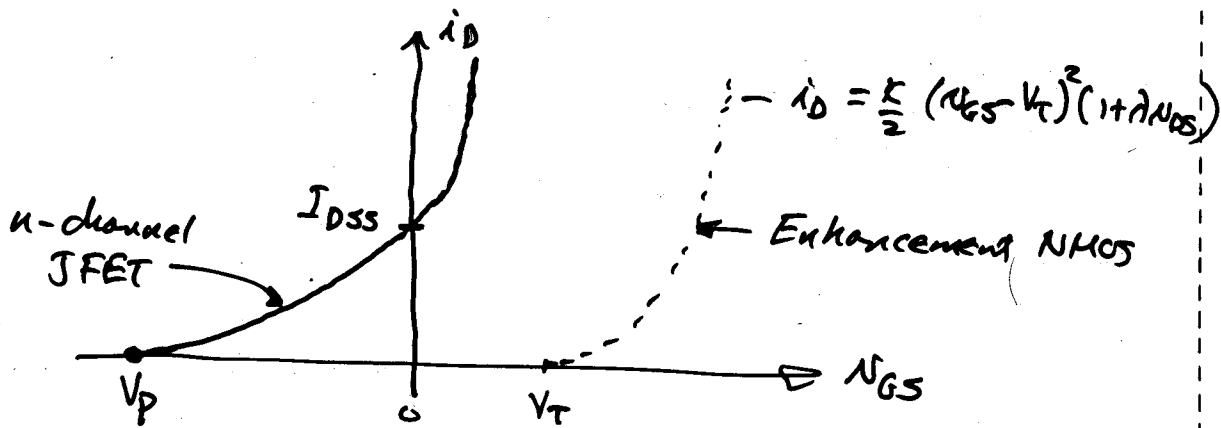
$$\therefore \frac{V_o}{V_s} = \frac{-g_m (r_o \parallel R_c \parallel R_L) (R_B \parallel r_{\pi})}{R_s + R_B \parallel r_{\pi}} = \frac{(-40 \text{ mS})(4.76 \text{ k})(2.22 \text{ k})}{3.22 \text{ k}} = \underline{\underline{-13.3 \frac{\text{V}}{\text{V}}}}$$

$$R_{out} = \left. \frac{V_x}{I_x} \right|_{V_s=0} = r_o \parallel R_c \parallel R_L = 100 \text{ k} \parallel 5 \text{ k} = \underline{\underline{4.76 \text{ k}}}$$

JFET S.S Model -



Transconductance Characteristics.

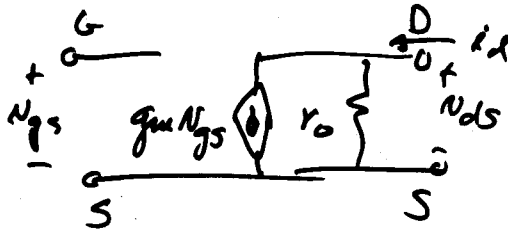


Q_{ABC} notation: A = terminal w. highest mag. of potential
 B = " " lowest " " "
 C = condition of the remaining terminal w.r.t. terminal B.

JFET Large signal model:
$$i_D = I_{DSS} \left[1 - \frac{V_{GS}}{V_p} \right]^2 (1 + \lambda V_{DS}), \quad V_{DS} > V_{GS} - V_p$$

Small signal model:

$$i_d = k_1 N_{gs} + k_2 N_{ds} = g_m N_{gs} + g_o N_{ds}$$



$$g_m = \left. \frac{i_d}{N_{gs}} \right|_{N_{ds}=0} = \left. \frac{\partial i_D}{\partial N_{gs}} \right|_Q = -\frac{2I_{DSS}}{V_p} \left(1 - \frac{V_{GS}}{V_p}\right) (1 + \lambda V_{DS})$$

Note that:

$$\left(1 - \frac{V_{GS}}{V_p}\right) = \sqrt{\frac{I_D}{I_{DSS}(1 + \lambda V_{DS})}}$$

$$g_m = \frac{2}{|V_p|} \sqrt{I_D I_{DSS}(1 + \lambda V_{DS})} \approx \frac{2}{|V_p|} \sqrt{I_D I_{DSS}}$$

$$\text{or, } g_m = -\frac{2I_{DSS}}{V_p^2} (V_p - V_{GS}) = \frac{2I_{DSS}}{V_p^2} (V_{GS} - V_p)$$

$$g_o = \left. \frac{i_d}{N_{ds}} \right|_{N_{gs}=0} \approx \left. \frac{\partial i_D}{\partial N_{ds}} \right|_Q = \lambda I_{DSS} \left[1 - \frac{V_{GS}}{V_p}\right]^2 = \frac{\lambda I_D}{1 + \lambda V_{DS}} \approx \lambda I_D \quad \text{if } \lambda V_{DS} \ll 1$$

$$g_m \approx \frac{2}{|V_p|} \sqrt{I_D I_{DSS}} \quad g_o \approx \lambda I_D$$

(Table 13.4)