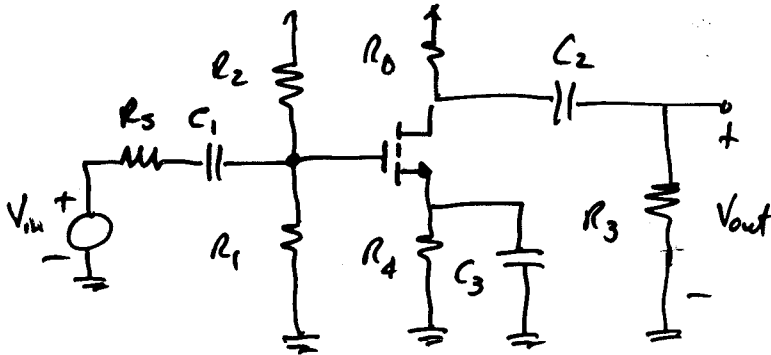
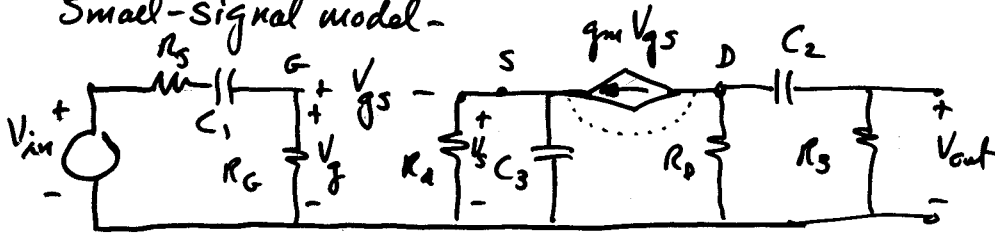


Warm-up Comments

MOSFET Example -



Small-signal model -



$$R_G = R_1 || R_2$$

1.) Direct analysis

$$\frac{V_{out}(s)}{V_{in}(s)} = \left( \frac{V_{out}}{V_{gs}} \right) \left( \frac{V_{gs}}{V_g} \right) \left( \frac{V_g}{V_{in}} \right)$$

$$\frac{V_{gs}}{V_g} : \quad V_{gs} = V_g - V_s = V_g - g_m V_{gs} Z_s$$

$$V_{gs} (1 + g_m Z_s) = V_g \Rightarrow \frac{V_{gs}}{V_g} = \frac{1}{1 + g_m Z_s}$$

$$\frac{V_{gs}}{V_g} = \frac{1}{1 + g_m \left( \frac{R_4 + 1/sC_3}{R_4 + 1/sC_3} \right)} = \frac{1}{1 + g_m \left( \frac{R_4}{sC_3 R_4 + 1} \right)} = \frac{sC_3 R_4 + 1}{sC_3 R_4 + 1 + g_m R_4}$$

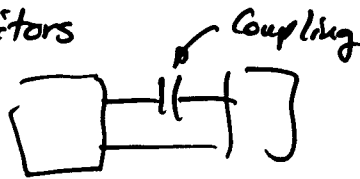
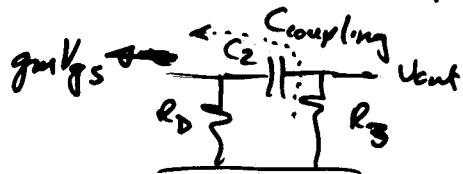
$$= \left( \frac{1}{1 + g_m R_4} \right) \left[ \frac{sC_3 R_4 + 1}{sC_3 R_4 + 1} \right]$$

Zero =  $-\frac{1}{R_4 C_3} = z_2$   
 Pole =  $-\frac{1 + g_m R_4}{C_3 R_4} = p_2$

$$\frac{V_{out}(s)}{V_{in}(s)} = MBG \times F_L(s) = MBG \left( \frac{s}{s+p_1} \right) \left( \frac{s+z_2}{s+p_2} \right) \left( \frac{s}{s+p_3} \right)$$

Types of Low Frequency Capacitors

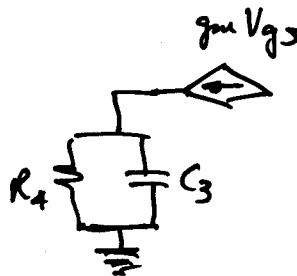
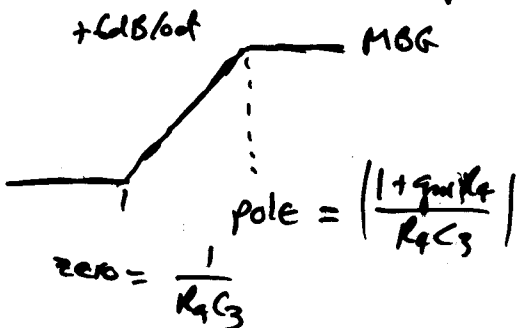
1.) Coupling  $\rightarrow \frac{s}{s+p}$



$$V_{out} = -g_m V_{gs} \left( \frac{R_D}{R_D + R_3 + \frac{1}{sC_2}} \right) R_3$$

$$\frac{V_{out}}{V_{gs}} = \frac{-g_m R_D R_3}{R_D + R_3 + \frac{1}{sC_2}} = \frac{-g_m R_D R_3 s}{s(R_D + R_3) + \frac{1}{C_2}} = \left( \frac{-g_m R_D R_3}{R_D + R_3} \right) \left( \frac{s}{s + \frac{1}{C_2(R_D + R_3)}} \right)$$

2.) Bypass  $\rightarrow \frac{s+z}{s+p}$



Back to the MOSFET Prob.

$$\omega_L = \omega_{-20dB} \text{ (lower)}$$

1.) Direct analysis

- a.) Bode plot
- b.) dominant
- c.)  $\sqrt{2} p_i^2 - 2 z z_k^2$

2.) Short-circuit time constant

- a.) If the C's are independent then the  $\frac{1}{R_{sc i} C_i} = |p_i|$
- b.)  $\omega_L \approx \sum_i \frac{1}{R_{sc i} C_i}$

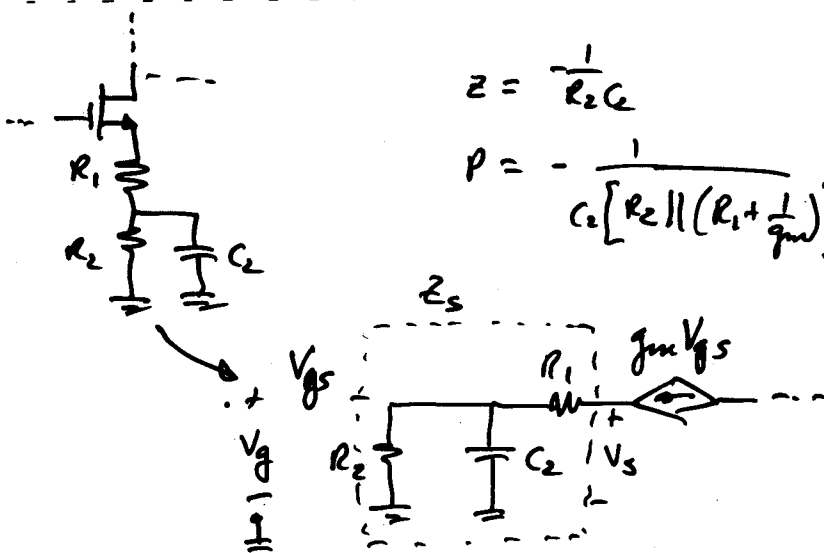
Comment: One approach good for quizzes is to use the S.C. time constant approach (when caps are indep.) to find poles and zeros.

Bypass cap.  $z = \frac{1}{R_i C_i}$

$R_i =$  bypassed resistance

$p = \frac{1}{R_{eq i} C_i}$

$R_{eq i} =$  resistance seen by  $C_i$



$$z = -\frac{1}{R_2 C_2}$$

$$p = -\frac{1}{C_2 \left[ R_2 \parallel \left( R_1 + \frac{1}{g_m} \right) \right]}$$

$$\frac{V_{gs}}{V_g} = \frac{1}{1 + g_m Z_s} = \frac{1}{1 + g_m \left[ R_1 + \frac{R_2}{s R_2 C_2 + 1} \right]}$$

$$= \frac{1}{1 + g_m R_1 + \frac{g_m R_2}{s R_2 C_2 + 1}} = \frac{s R_2 C_2 + 1}{(1 + g_m R_1) s R_2 C_2 + (1 + g_m R_1) + g_m R_2}$$

$$= \left( \frac{1}{1 + g_m R_1} \right) \left( \frac{s R_2 C_2 + 1}{s R_2 C_2 + 1 + \frac{g_m R_2}{1 + g_m R_1}} \right)$$

$$p = ? \quad - \left( 1 + \frac{g_m R_2}{1 + g_m R_1} \right) \frac{1}{R_2 C_2}$$

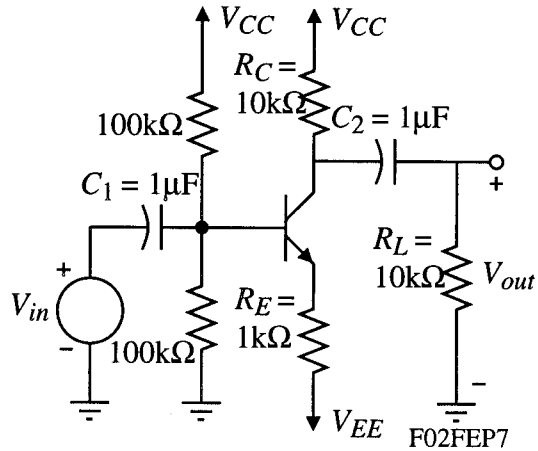
$$p = -\frac{1}{R_2 C_2} \left( \frac{1 + g_m R_1 + g_m R_2}{1 + g_m R_1} \right) = -\frac{1}{R_2 C_2} \left[ \frac{\frac{1}{g_m} + R_1 + R_2}{\frac{1}{g_m} + R_1} \right]$$

✓

Low Frequency Example (Not covered in class)

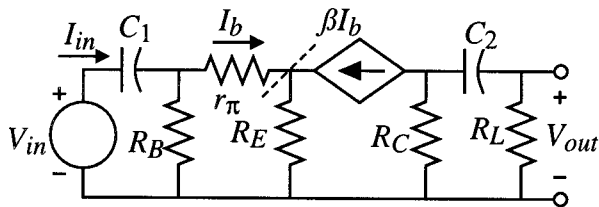
A BJT amplifier is shown. Assume that the BJT has the small signal parameters of  $g_m = 50\text{mA/V}$ ,  $r_\pi = 2\text{k}\Omega$ , and  $r_o = \infty$ .

- Find the midband voltage gain of this amplifier,  $V_{out}/V_{in}$ .
- Find the numerical value of all poles and zeros of the low frequency response.
- Find the value of the lower -3dB frequency,  $f_L$ , in Hz.

Solution

The low-frequency, small signal model for this problem is shown where  $R_B = 50\text{k}\Omega$ .

The algebraic approach to this problem is:



$$\begin{aligned} \frac{V_{out}}{V_{in}} &= \left( \frac{V_{out}}{I_b} \right) \left( \frac{I_b}{I_{in}} \right) \left( \frac{I_{in}}{V_{in}} \right) = \left( \frac{-\beta R_L R_C}{R_C + R_L + \frac{1}{sC_2}} \right) \left( \frac{R_B}{R_B + r_\pi + (1+\beta)R_E} \right) \left( \frac{1}{\frac{1}{sC_1} + R_B \parallel [r_\pi + (1+\beta)R_E]} \right) \\ &= \left( \frac{-\beta R_L R_C}{(R_C + R_L)[r_\pi + (1+\beta)R_E]} \right) \left( \frac{s}{s + \frac{1}{C_2(R_C + R_L)}} \right) \left( \frac{s}{s + \frac{1}{C_1(R_B \parallel [r_\pi + (1+\beta)R_E])}} \right) \\ &= \frac{-100 \cdot 10\text{K} \cdot 10\text{K}}{20\text{K} \cdot 103\text{K}} \left( \frac{s}{s+50} \right) \left( \frac{s}{s+29.7} \right) = -4.854 \left( \frac{s}{s+50} \right) \left( \frac{s}{s+29.7} \right) \end{aligned}$$

The midband gain is  $\boxed{MBG = 4.854 \text{ V/V}}$

$$\therefore \omega_L \approx \sqrt{(29.7)^2 + (50)^2} = 58.2 \text{ rads/sec.} \rightarrow \boxed{f_L = 9.26\text{Hz}}$$

The poles and zeros are,

$\boxed{\text{Two zeros at } s = 0, \text{ a pole at } s = -29.7 \text{ rads/sec. and a pole at } s = -50 \text{ rads/sec.}}$