Homework Assignment No. 2 - Solutions

Problem 1 - (10 points)

 $\downarrow V_{CC}$ $\downarrow V_{IN}$ $\downarrow V_{IN}$ $\downarrow V_{IN}$ $\downarrow Q1$ $\downarrow Q1$ $\downarrow Q1$ $\downarrow Q1$ $\downarrow R_L \swarrow V_{OUT}$ $\downarrow Q2$ $\downarrow -$ Fig. 040-09

a) For the emitter follower output stage shown below, find the value of R_1 for maximum efficiency and find the value of that efficiency. $V_{CC} = -V_{EE} = 2.5$ V, $V_{CE}(sat) = 0.2$ V, $R_L = 10$ k Ω , $V_{BE}(on) = 0.7$ V.

b) The load resistance R_L is replaced with a capacitor of 100pF. If the input voltage suddenly drops from 2.5V to -2.5V, explain what happens at the output and accurately sketch the output voltage as a function of time, specifying its initial and final values and time interval.

<u>Solution</u>

The I_O for maximum efficiency is found as,

$$\begin{split} I_Q &= \left(\frac{V_{CC} - V_{CE}(sat)}{R_L}\right) = 230 \mu A \\ R_I &= \left(\frac{-V_{EE} - V_{BE}}{I_Q}\right) = 7.826 \mathrm{k} \Omega \\ P_L(\max) &= \left(\frac{V_{CC} - V_{CE}(sat)}{\sqrt{2}}\right) \left(\frac{I_Q}{\sqrt{2}}\right) = 0.5(2.3\mathrm{V})(0.23\mathrm{mA}) = 0.2645 \mathrm{mW} \\ P_{supply} &= 2V_{CC}I_Q = 2(2.5)(0.23\mathrm{mA}) = 1.15\mathrm{mW} \\ \eta &= \frac{P_{L(\max)}}{P_{\sup ply}} = \frac{1}{4} \left(1 - \frac{V_{CE}(sat)}{V_{CC}}\right) = 23\% \end{split}$$

b) The output would slew under such condition. The current will be limited by the bias current:

Slew rate=0.23mA/100pF=2.3V/µs



Problem 2 - (10 points)

Six versions of a source follower are shown below. Assume that $K'_N = 2K'_P$, $\lambda_P = 2\lambda_N$, all W/L ratios of all devices are equal, and that all bias currents in each device are equal. Neglect bulk effects in this problem and assume no external load resistor. Identify which circuit or circuits have the following characteristics: (a.) highest small-signal voltage gain, (b.) lowest small-signal voltage gain, (c.) the highest output resistance, (d.) the lowest output resistance, (e.) the highest $v_{out}(\max)$ and (f.) the lowest $v_{out}(\max)$.



(c.) and (d.) - Output resistance.

The denominators of the first table show the following:

Ckt.6 has the highest output resistance and Ckt. 1 the lowest output resistance.

(e.) Assuming no current has to be provided by the output, circuits 2, 4, and 6 can pull the output to V_{DD} . \therefore | Circuits 2, 4 and 6 have the highest output swing.

(f.) Assuming no current has to be provided by the output, circuits 1, 3, and 5 can pull the output to ground. \therefore | Circuits 1, 3 and 5 have lowest output swing.

Summary

(a.) Ckt. 5 has the highest voltage gain

(d.) Ckt. 1 has the lowest output resistance (e.) Ckts. 2,4 and 6 have the highest output

(b.) Ckt. 4 has the lowest voltage gain

(c.) Ckt. 6 has the highest output resistance (f.) Ckts. 1,3 and 5 have the lowest output

Problem 3 - (10 points)

A push-pull follower is shown which uses an NPN BJT and a p-channel MOSFET. In this problem, ignore the bulk effect, the channel length modulation, and the Early voltage. The parameters for the NPN BJT are $\beta_F =$ 100, $I_s =$ 10fA and $V_t = 25.9$ mV. The model parameters for the PMOS are $K_P' = 50\mu A/V^2$ and $V_T =$ -0.7V. (a.) Find the value of the dc batteries, V_1 and V_2 , which will cause 100 μ A to flow in Q1 and M2 when the dc value of $v_{IN} = 0$ VDC. (b.) Find the smallsignal input resistance, output resistance and voltage gain when the dc value of $v_{IN} = 0$ VDC.



Solution

(a.)
$$V_1 = V_{BE1} = V_t \ln\left(\frac{i_C}{I_s}\right) = 0.0259 \ln\left(\frac{100\mu A}{10fA}\right) = 0.5964 V$$
 _ $V_1 = 0.5964 V$ _ $V_2 = V_{SG2} = \sqrt{\frac{2I_D}{K_P'(W/L)}} + |V_{TP}| = \sqrt{\frac{2\cdot100}{50\cdot100}} + 0.7 = 0.9 V$ _ $V_2 = 0.9 V$ _ $V_2 = 0.9 V$

(b.) Small-signal model (simplified):

$$g_{m1} = \frac{I_{C1}}{V_t} = \frac{100\mu A}{25.9\text{mV}} = 3.86\text{mS}$$

$$r_{\pi 1} = \frac{1+\beta_F}{g_{m1}} = 26.159\text{k}\Omega$$

$$B1 = G2 + \sqrt{v_{\pi}} - E1 = S2$$

$$v_{in}$$

$$g_{m1}v_{\pi}$$

$$g_{m2}v_{gs}$$

$$C1 = D2$$

$$S01E1S1$$

$$g_{m2} = \sqrt{\frac{2K_P'W_2I_{D2}}{L_2}} = \sqrt{2 \cdot 50 \cdot 100 \cdot 100} = 1 \text{mS}$$

$$R_{in}: v_{in} = r_{\pi 1}i_{in} + (i_{in} + g_{m1}v_{\pi} + g_{m2} v_{gs2})R_L = r_{\pi 1}i_{in} + (i_{in} + g_{m1}r_{\pi 1}i_{in} + g_{m2} r_{\pi 1}i_{in})R_L$$

$$R_{in} = \frac{v_{in}}{i_{in}} = r_{\pi 1} + R_L + g_{m1}r_{\pi 1}R_L + g_{m2} r_{\pi 1}R_L = r_{\pi 1} + R_L(1+\beta_F) + g_{m2} r_{\pi 1}R_L$$

$$\therefore R_{in} = 26.159 \text{k}\Omega + 101 \cdot 100\Omega + 1 \cdot 26.159 \text{k}\Omega \cdot 0.1 = 38.875 \text{k}\Omega$$

$$R_{in} = 38.875 \text{k}\Omega$$

Problem 4 - (10 points)

Find an algebraic expression for the voltage gain, v_{out}/v_{in} , and the output resistance, R_{out} , of the source follower shown in terms of the small-signal model parameters, g_m and R_L (ignore r_{ds}). If the bias current is 1mA find the numerical value of the voltage gain and the output resistance. Assume that $K_N' = 110\mu A/V^2$, $V_{TN} = 0.7V$, and $K_P' = 50\mu A/V^2$, $V_{TP} = -0.7V$.

<u>Solution</u>

A small-signal model for this circuit is shown below neglecting r_{ds} of the transistors.



$$g_{m1}(v_{out} - v_{in}) \left(1 + \frac{g_{m3}}{g_{m2}}\right) = G_L v_{out}$$

$$\cdot \cdot \frac{v_{out}}{v_{in}} = \frac{g_{m1}\left(1 + \frac{g_{m3}}{g_{m2}}\right)}{g_{m1}\left(1 + \frac{g_{m3}}{g_{m2}}\right) + G_L}$$

Setting $\overline{v_{in}} = 0$ and applying i_t and solving for v_{out} and ignoring R_L gives,

$$i_t = g_{m3}v_{gs3} + g_{m1}v_{out} = g_{m3}\left(\frac{g_{m1}}{g_{m2}}\right)v_{out} + g_{m1}v_{out}$$
$$\therefore \qquad \frac{v_{out}}{i_t} = \boxed{R_{out} = \frac{1}{g_{m1}\left(1 + \frac{g_{m3}}{g_{m2}}\right)}}$$

Note that the 1mA splits between M1(M2) and M3 in a ratio of 1 to 100. Therefore, $I_{D1} = I_{D2} = 9.9 \mu A$ and $I_{D3} = 990.1 \mu A$.

$$\therefore g_{m1} = \sqrt{2 \cdot 110 \cdot 100 \cdot 9.9} = 466.71 \mu \text{S}, g_{m2} = \sqrt{2 \cdot 50 \cdot 1 \cdot 9.9} = 31.47 \mu \text{S}$$

and $g_{m3} = \sqrt{2 \cdot 110 \cdot 100 \cdot 990.1} = 3146.7 \mu \text{S}$
$$\frac{v_{out}}{v_{in}} = \frac{466.71 \cdot 101}{466.71 \cdot 101 + 1/50} = \frac{47.137}{47.137 + 20} = \underline{0.702 \text{ V/V}}$$
$$R_{out} = \frac{1000}{47.137} = \underline{21.2\Omega}$$



Summing currents at the output node gives,

$$g_{m1}v_{gs1} = g_{m3}v_{gs3} + G_Lv_{out}$$

Also, $v_{gs3} = -g_{m1}v_{gs1}(1/g_{m2})$
 $\therefore \qquad g_{m1}v_{gs1} = g_{m3}\left(-\frac{g_{m1}}{g_{m2}}\right)v_{gs1} + G_Lv_{out}$
 $g_{m1}v_{gs1}\left(1 + \frac{g_{m3}}{g_{m2}}\right) = G_Lv_{out} \rightarrow$