

## Homework Assignment No. 7 -Solutions

### Problem 1 - (10 points)

Find the low frequency PSRR and all roots of the positive and negative power supply rejection ratio performance for the two-stage op amp of Fig. P6.3-9.

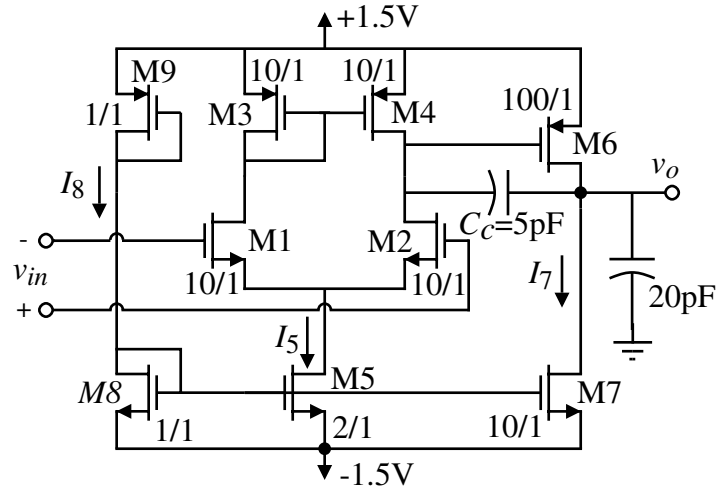


Figure P6.3-10

### Solution

Referring to the figure

$$V_{DD} - V_{SS} = V_{T8} + V_{T9} + \sqrt{\frac{2I_8}{K_N(W/L)_8}} + \sqrt{\frac{2I_8}{K_P(W/L)_9}}$$

or,  $I_8 = 60 \mu A$

Now,

$$g_{m1} = 363.3 \mu S, g_{ds2} = 2.4 \mu S, g_{ds4} = 3 \mu S, g_{m6} = 774.6 \mu S, g_{ds6} = 30 \mu S$$

and  $g_{ds7} = 24 \mu S$

$$\therefore A_{v1} = 67.3 \text{ and } A_{v2} = 14.3$$

For the positive PSRR, the low frequency PSRR is

$$PSRR^+ = \frac{A_v(0)G_{II}}{g_{ds6}} = 1737$$

and poles and zeros are

$$p_1 = \frac{(GB)g_{ds6}}{A_v(0)G_{II}} = 6.66 \text{ KHz}, z_1 = GB = 11.6 \text{ MHz. and } z_2 = p_2 = 6.2 \text{ MHz.}$$

For the negative PSRR, the low frequency PSRR is given by

$$PSRR^- = \frac{A_v(0)G_{II}}{g_{ds7}} = 2171$$

and the poles and zeros are

$$p_1 = \frac{(GB)G_I}{g_{m1}} = 172.4 \text{ KHz}, z_1 = GB = 11.6 \text{ MHz and } z_2 = p_2 = 6.2 \text{ MHz.}$$

**Problem 2 – (10 points)**

A CMOS op amp that uses a 5V power supply is shown. All transistor lengths are  $1\mu\text{m}$  and operate in the saturation region. Design all of the W values of every transistor of this op amp to meet the following specifications: Slew rate =  $\pm 10\text{V}/\mu\text{s}$ ,  $V_{\text{out(max)}} = 4\text{V}$ ,  $V_{\text{out(min)}} = 1\text{V}$ ,  $V_{\text{ic(min)}} = 1.5\text{V}$ ,  $V_{\text{ic(max)}} = 4\text{V}$  and  $\text{GB} = 10\text{MHz}$ .

Your design should meet or exceed these specifications. Ignore bulk effects and summarize your W values to the nearest micron, the bias current,  $I_5(\mu\text{A})$ , the power dissipation, the differential voltage gain,  $A_{vd}$ , and  $V_{BP}$  and  $V_{BN}$  in the table shown.

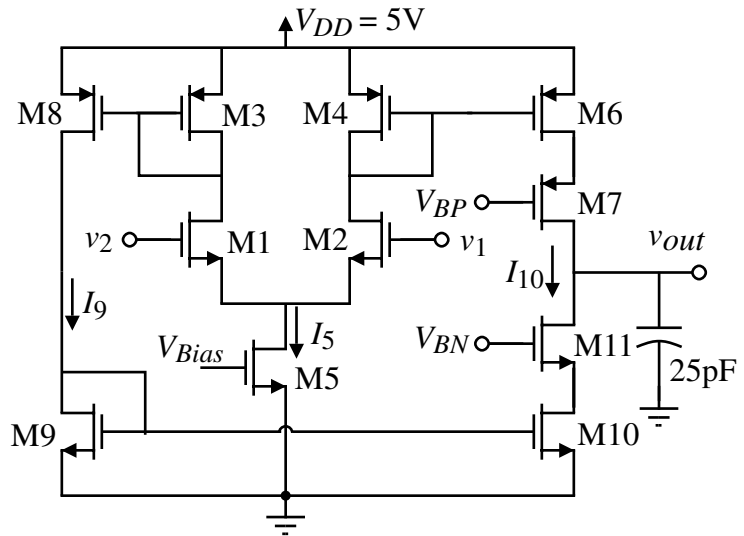


Figure P6.5-13

**Solution**

$$1.) I_5 = C_L \cdot SR = 250\mu\text{A}$$

$$2.) g_{m1} = \text{GB} \cdot C_L = 20\pi \times 10^6 \cdot 25\text{pF} = 1,570.8\mu\text{S} \Rightarrow \frac{W_1}{L_1} = \frac{(1.570 \times 10^{-3})^2}{2 \cdot 110 \cdot 125 \times 10^{-6}} = 90$$

$$3.) W_3=W_4=W_6=W_7=W_8 = \frac{2I_D}{K'(V_{DS}(\text{sat}))^2} = \frac{2 \cdot 250}{50 \cdot 0.25} = 40 \quad (\text{assumed } I_D \text{ of } 250\mu\text{A} \text{ worst case})$$

$$4.) W_9=W_{10}=W_{11} = \frac{2I_D}{K'(V_{DS}(\text{sat}))^2} = \frac{2 \cdot 250}{110 \cdot 0.25} = 18 \quad (\text{assumed } I_D \text{ of } 250\mu\text{A} \text{ worst case})$$

$$5.) V_{\text{icm(min)}} = V_{DS5}(\text{sat}) + V_{GS1} \rightarrow V_{DS5}(\text{sat}) = 1.5 - (0.159 + 0.7) = 0.6411\text{V}$$

$$\therefore W_5 = \frac{2I_D}{K'(V_{DS}(\text{sat}))^2} = \frac{2 \cdot 250}{110 \cdot 0.6411^2} = 11$$

$$6.) A_{vd} = g_{m1} R_{\text{out}} \quad g_{mN} = 704\mu\text{S}, r_{dsN} = 0.2\text{M}\Omega, g_{mP} = 707\mu\text{S}, r_{dsP} = 0.16\text{M}\Omega$$

$$R_{\text{out}} \approx g_{mN} \cdot r_{dsN}^2 \parallel g_{mP} \cdot r_{dsP}^2 = 28.14\text{M}\Omega \parallel 18.1\text{M}\Omega = 11\text{M}\Omega$$

$$\therefore A_{vd} = 1.57\text{mS} \cdot 11\text{M}\Omega = 17,329\text{V/V}$$

$$7.) V_{BP} = 5 - V_{DSP}(\text{sat}) + V_{GSP}(\text{sat}) = 5 - 0.5 + 0.5 + 0.7 = 3.3\text{V}$$

$$V_{BN} = V_{DSP}(\text{sat}) + V_{GSP}(\text{sat}) = 0.5 + 0.5 + 0.7 = 1.7\text{V}$$

$$8.) P_{\text{diss}} = 5(250\mu\text{A} + 250\mu\text{A}) = 2.5\text{mW}$$

W1=W2	W3=W4=W6 =W7=W8	W9=W10 =W11	W5	$I_5(\mu\text{A})$	$A_{vd}$	$V_{BP}$	$V_{BN}$	$P_{\text{diss}}$
90 $\mu\text{m}$	40 $\mu\text{m}$	18 $\mu\text{m}$	11 $\mu\text{m}$	250 $\mu\text{A}$	17,329 V/V	3.3V	1.7V	2.5mW

## Problem 3 - (10 points)

6.15

$$200 \mu\text{A} - |I_{D_2}| - |I_{D_3}| - |I_{D_4}| = I_{D_1}$$

$$100 \mu\text{A} = I_{D_1} = I_{D_2} = I_{D_3} = I_{D_4}$$

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}} = \frac{3.9 (8.85 \times 10^{-14} \text{ F/cm})}{80 \text{ \AA}}$$

$$= 431 \text{ nF/cm}^2$$

$$\mu_n C_{ox} = \frac{450 \text{ cm}^2}{\text{V}\cdot\text{s}} \cdot 431 \frac{\text{nF}}{\text{cm}^2}$$

$$= 194 \mu\text{A/V}^2$$

$$k'_n = 194 \mu\text{A/V}^2$$

$$k'_p = 64.7 \mu\text{A/V}^2$$

$$\frac{v_o}{v_i} = -g_{m_2} (r_{o_2} \parallel r_{o_4}) g_{m_6} (r_{o_6} \parallel r_{o_7})$$

$$\frac{1}{r_{o_2}} = \frac{I_{D_2}}{L_{eff}} \frac{dX_d}{dV_{DS}} = \frac{100 \mu\text{A}}{0.72 \mu\text{m}} (0.04 \mu\text{m}) = 5.56 \mu\text{A}$$

$$r_{o_2} = 180 \text{ k}\Omega = r_{o_4}$$

$$r_{o_6} = 90 \text{ k}\Omega = r_{o_7}$$

$$L_{eff} = L - X_d - 2L_d$$

$$= 1 - 0.1 - 2(0.09)$$

$$= 0.72 \mu\text{m}$$

$$g_{m_2} = \sqrt{2 k'_p \frac{W}{L_{eff}} I_{D_2}}$$

$$= \sqrt{2 (64.7 \mu\text{A/V}^2) \left(\frac{150}{0.72}\right) (100 \mu\text{A})}$$

$$= 1640 \mu\text{A/V}$$

$$g_{m_6} = \sqrt{2 (194 \mu\text{A/V}^2) \left(\frac{100}{0.72}\right) (200 \mu\text{A})}$$

$$= 3280 \mu\text{A/V}$$

$$\frac{v_o}{v_i} = -(1.64 \text{ m}) (90 \text{ k}) (3.28 \text{ m}) (45 \text{ k})$$

$$= -2.18 \times 10^4$$

common mode range :

From (6.75),

$$V_{ic} > V_{t_1} + V_{t_3} + V_{ov_3} - V_{SS}$$

$$V_{ov_3} = \sqrt{\frac{2(100)}{194 (50/0.72)}} = 0.12 \text{ V}$$

$$V_{ic} > -0.8 + 0.6 + 0.12 - 1.5$$

$$V_{ic} > -1.58 \text{ V}$$

From (6.77),

$$V_{ic} < V_{t_1} + V_{ov_1} + V_{ov_5} + V_{DD}$$

$$V_{ov_5} = -\sqrt{\frac{2(200)}{64.7 (150/0.72)}} = -0.17 \text{ V}$$

$$V_{ov_1} = -\sqrt{\frac{2(100)}{64.7 (150/0.72)}} = -0.12 \text{ V}$$

$$V_{ic} < -0.8 - 0.12 - 0.17 + 1.5$$

$$V_{ic} < 0.41 \text{ V}$$

From (6.86),

$$\frac{v_o}{v_{dd}} \equiv 0$$

From (6.87),

$$\frac{v_o}{v_{SS}} = \frac{r_{o_7}}{r_{o_6} + r_{o_7}} = 0.5$$

## Problem 3 – Continued

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TWO-STAGE CMOS AMPLIFIER
*****
VDD 100 0 1.5
VSS 200 0 -1.5
M1 7 5 4 4 PMOS W=1500 L=10
M2 8 6 4 4 PMOS W=1500 L=10
M3 7 7 100 100 NMOS W=500 L=10
M4 8 7 100 100 NMOS W=500 L=10
M5 4 3 100 100 PMOS W=1500 L=10
M6 5 8 100 100 NMOS W=1000 L=10
M7 9 3 100 100 PMOS W=1500 L=10
M8 3 3 100 100 PMOS W=1500 L=10
IRMS1 1 100 1000
+ THE DC OFFSET IS ADJUSTED BY TRIAL AND ERROR
+ TO SET THE OUTPUT TO ZERO.
V11 5 3 4.5V
V12 4 3 0
V13 3 3 0
*GSPY = GMINV - 2LS -ID = 1 - 2(0.05) = 0.1 = 0.12 CM
*GAMBIA=(GMINV)/GSPY = 0.0010707 = 0.001
.MODEL PMS1 PMS LEVEL=1 KP=1000 VTO=0.5 LAMBDA=0.001
.MODEL PMS2 PMS LEVEL=1 KP=1000 VTO=0.5 LAMBDA=0.001
.OPTIONS SUPPLY BONES
.ENDC
.ENDC
.OP
.OP V11 V12
.END

**** OPERATING POINT INFORMATION FROM= 17.000 TIME= 07.000
NODE      +VOLTAGE      NODE      +VOLTAGE      NODE      +VOLTAGE
+013      = 0.          013      = 0.004E-01  014      = 0.007E-01
+015      = 4.400E-02  015      = 0.          017      = -7.400E-01
+018      = -7.400E-01  018      = 0.004E-04  019      = 1.000E-00
+0100     = -1.000E-00

SUBCIRCUIT
ELEMENTS 0:01  0:02  0:03  0:04
MODEL 0:0000  0:0000  0:0000  0:0000
ID      -0.770E-05  -0.770E-05  0.770E-05  0.770E-05
IB      0.          0.          0.          0.
IIO     1.400E-04  1.400E-04  -7.000E-15  -7.000E-15
VDS    -0.107E-01  -0.107E-01  7.000E-01  7.000E-01
VDS    -1.400E+00  -1.400E+00  7.000E-01  7.000E-01
VDS    0.          0.          0.          0.
VDS    -0.000E-01  -0.000E-01  0.000E-01  0.000E-01
VDSAT   -1.007E-01  -0.107E-01  1.000E-01  1.000E-01
BETA    1.000E-02  1.000E-02  1.000E-02  1.000E-02
GAIN EFF 0.          0.          0.          0.
GM      1.400E-03  1.400E-03  1.400E-03  1.400E-03
CDS     4.000E-04  4.000E-04  0.000E-04  0.000E-04
CDS     0.          0.          0.          0.

SUBCIRCUIT
ELEMENTS 0:05  0:06  0:07  0:08
MODEL 0:0000  0:0000  0:0000  0:0000
ID      -1.054E-04  1.054E-04  -2.000E-04  -2.000E-04
IB      0.          0.          0.          0.
IIO     0.443E-15  -1.000E-14  1.000E-04  0.000E-14
VDS    -0.070E-01  7.000E-01  -0.070E-01  -0.070E-01
VDS    -0.443E-01  1.000E+00  -0.443E-01  -0.070E-01
VDS    0.          0.          0.          0.
VDS    -0.000E-01  0.000E-01  -0.000E-01  -0.000E-01
VDSAT   -1.070E-01  1.000E-01  -0.070E-01  -0.070E-01
BETA    1.000E-02  1.000E-02  1.000E-02  1.000E-02
GAIN EFF 0.          0.          0.          0.
GM      1.070E-03  1.070E-03  1.070E-03  1.070E-03
CDS     1.000E-05  1.000E-05  1.000E-05  1.000E-05
CDS     0.          0.          0.          0.

**** SMALL-SIGNAL TRANSFER CHARACTERISTICS
V(1)/V(1) = -0.070E+00
INPUT RESISTANCE AT V(1) = 1.000E+00
OUTPUT RESISTANCE AT V(1) = 4.750E+04

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TWO-STAGE CMOS AMPLIFIER (SMALL-SIGNAL COMMON-MODE INPUT VOLTAGE)
*****
VDD 100 0 1.5
VSS 200 0 -1.5
M1 7 5 4 4 PMOS W=1500 L=10
M2 8 6 4 4 PMOS W=1500 L=10
M3 7 7 100 100 NMOS W=500 L=10
M4 8 7 100 100 NMOS W=500 L=10
M5 4 3 100 100 PMOS W=1500 L=10
M6 5 8 100 100 NMOS W=1000 L=10
M7 9 3 100 100 PMOS W=1500 L=10
M8 3 3 100 100 PMOS W=1500 L=10
IRMS1 1 100 1000
+ THE DC OFFSET IS ADJUSTED BY TRIAL AND ERROR
+ TO SET THE OUTPUT TO ZERO.
V11 5 3 10.7V
V12 4 3 0
* THE MAXIMUM VALUE OF VDC IS ADJUSTED BY TRIAL AND ERROR
+ UNTIL NO MARKET OPERATES IN THE ACTIVE REGION
+ (CHECK [VDC] > [VDSAT] FOR ME)
VDC 1 0 0.2V
*GSPY = GMINV - 2LS -ID = 1 - 2(0.05) = 0.1 = 0.12 CM
*GAMBIA=(GMINV)/GSPY = 0.0010707 = 0.001
.MODEL PMS1 PMS LEVEL=1 KP=1000 VTO=0.5 LAMBDA=0.001
.MODEL PMS2 PMS LEVEL=1 KP=1000 VTO=0.5 LAMBDA=0.001
.OPTIONS SUPPLY BONES
.ENDC
.ENDC
.OP
.OP V11 V12
.END

**** OPERATING POINT INFORMATION FROM= 17.000 TIME= 17.000
NODE      +VOLTAGE      NODE      +VOLTAGE      NODE      +VOLTAGE
+013      = 0.000E-01  013      = 0.004E-01  014      = 1.000E+00
+015      = 0.000E-01  015      = 0.000E-01  017      = -1.000E-01
+018      = -7.400E-01  018      = 1.000E-04  019      = 1.000E+00
+0100     = -1.000E+00

SUBCIRCUIT
ELEMENTS 0:01  0:02  0:03  0:04
MODEL 0:0000  0:0000  0:0000  0:0000
ID      -0.000E-00  -0.000E-00  0.000E-00  0.000E-00
IB      0.          0.          0.          0.
IIO     1.000E-14  1.000E-14  -7.000E-15  -7.000E-15
VDS    -0.000E-01  -0.000E-01  7.000E-01  7.000E-01
VDS    -1.000E+00  -1.000E+00  7.000E-01  7.000E-01
VDS    0.          0.          0.          0.
VDS    -0.000E-01  -0.000E-01  0.000E-01  0.000E-01
VDSAT   -1.000E-01  -1.000E-01  1.000E-01  1.000E-01
BETA    1.000E-02  1.000E-02  1.000E-02  1.000E-02
GAIN EFF 0.          0.          0.          0.
GM      1.000E-03  1.000E-03  1.000E-03  1.000E-03
CDS     0.000E-00  0.000E-00  0.000E-00  0.000E-00
CDS     0.          0.          0.          0.

SUBCIRCUIT
ELEMENTS 0:05  0:06  0:07  0:08
MODEL 0:0000  0:0000  0:0000  0:0000
ID      -1.000E-04  1.000E-04  -2.000E-04  -2.000E-04
IB      0.          0.          0.          0.
IIO     0.000E-00  -1.000E-14  1.000E-04  0.000E-00
VDS    -0.000E-01  7.000E-01  -0.000E-01  -0.000E-01
VDS    -0.000E-01  1.000E+00  -0.000E-01  -0.000E-01
VDS    0.          0.          0.          0.
VDS    -0.000E-01  0.000E-01  -0.000E-01  -0.000E-01
VDSAT   -1.000E-01  1.000E-01  -0.000E-01  -0.000E-01
BETA    1.000E-02  1.000E-02  1.000E-02  1.000E-02
GAIN EFF 0.          0.          0.          0.
GM      1.000E-03  1.000E-03  1.000E-03  1.000E-03
CDS     0.000E-00  0.000E-00  0.000E-00  0.000E-00
CDS     0.          0.          0.          0.

**** SMALL-SIGNAL TRANSFER CHARACTERISTICS
V(1)/V(1) = -2.000E+00
INPUT RESISTANCE AT V(1) = 1.000E+00
OUTPUT RESISTANCE AT V(1) = 4.750E+04

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## Problem 3 – Continued

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TWO-STAGE CMOS AMPLIFIER (GAIN FROM VGS)
*****
VDD 100 0 1.5
VSS 100 0 -1.5
M1 7 0 4 4 PMOS W=1500 L=10
M2 8 4 4 4 PMOS W=1500 L=10
M3 7 7 200 200 NMOS W=500 L=10
M4 8 7 200 200 NMOS W=500 L=10
M5 4 3 100 100 PMOS W=1500 L=10
M6 5 8 200 200 NMOS W=500 L=10
M7 5 3 100 100 PMOS W=1500 L=10
M8 3 3 200 200 PMOS W=1500 L=10
IRIAS 3 100 2000
* THE DC OFFSET IS ADJUSTED BY TRIAL AND ERROR
* TO GET THE OUTPUT TO ZERO.
VIL 5 3 4.00
VIO 4 3 0
+ THE BIASING VALUE OF VTC IS ADJUSTED BY TRIAL AND ERROR
+ ONLY A SINGLE OPERATOR IN THE BIASING SECTION
+ GAIN=[VGS] * [VDSAT] FOR M1)
VTC 3 0 -1.50
+GAIN = LGAIN - 2LD -GD = 1 - 2(0.00) - 0.1 = 0.70 OM
+LAMBDA=(IDC/IDDC)/GAIN = 0.040/0.10 = 0.0004
.MODEL MOSFET LEVEL=1 KP=0.040 VTO=0.5 LAMBDA=0.0004
.MODEL PMOS PMOS LEVEL=1 KP=0.040 VTO=-0.5 LAMBDA=0.0004
.OPTIONS MESSAGE NONE
.MIXER OFF=0
.OPTIONS VTCOL=IN ANTIOL=IF BISTOL=00
.OFF
.OP VGS VIL
.END

**** OPERATING POINT INFORMATION TRNS= 27.000 TRNS= 27.000
NODE      +VOLTAGE      NODE      +VOLTAGE      NODE      +VOLTAGE
+0:1      =-1.500E+00  0:1      = 3.000E-01  0:8      =-1.500E-01
+0:5      =-1.500E+00  0:5      =-1.500E+00  0:7      =-7.500E-01
+0:8      =-7.500E-01  0:8      = 3.000E-04  0:100     = 1.500E-03
+0:100    =-1.500E-03

**** MESSAGE
*****
SUBCIRCUIT
ELEMENT 0:R1 0:R2 0:R3 0:R4
MODEL 0:R1000 0:R2000 0:R3000 0:R4000
R1 0 -1.500E-04 -1.500E-04 1.000E-04 1.000E-04
R2 0 0 0 0
R3 1.500E-15 1.500E-15 -7.500E-15 -7.500E-15
R4 -7.500E-01 -7.500E-01 7.500E-01 7.500E-01
R5 -1.500E-01 -1.500E-01 7.500E-01 7.500E-01
R6 0 0 0 0
R7 -8.000E-01 -8.000E-01 8.000E-01 8.000E-01
RDSAT 8.000E-01 -1.500E-01 1.500E-01 1.500E-01
RSTA 8.000E-01 7.500E-01 1.500E-01 1.500E-01
GDS OFF 0 0 0 0
G1 1.500E-01 1.500E-01 1.500E-01 1.500E-01
G2 1.500E-01 1.500E-01 1.500E-01 1.500E-01
G3 0 0 0 0

SUBCIRCUIT
ELEMENT 0:R5 0:R6 0:R7 0:R8
MODEL 0:R1000 0:R2000 0:R3000 0:R4000
R5 0 -2.100E-04 2.100E-04 -2.100E-04 -2.100E-04
R6 0 0 0 0
R7 2.100E-14 -2.100E-14 1.500E-14 1.500E-14
R8 -8.000E-01 7.500E-01 -8.000E-01 -8.000E-01
R9 -2.100E+00 1.500E+00 -1.500E+00 -1.500E+00
R10 0 0 0 0
R11 -8.000E-01 8.000E-01 -8.000E-01 -8.000E-01
RDSAT -1.500E-01 1.500E-01 -1.500E-01 -1.500E-01
RSTA 1.500E-01 1.500E-01 1.500E-01 1.500E-01
GDS OFF 0 0 0 0
G1 1.500E-01 1.500E-01 1.500E-01 1.500E-01
G2 1.500E-01 1.500E-01 1.500E-01 1.500E-01
G3 0 0 0 0

**** SMALL-SIGNAL TRANSFER CHARACTERISTICS
VGS/VIL = -1.500E-04
INPUT RESISTANCE AT VIL = 1.500E+00
OUTPUT RESISTANCE AT VGS = 4.750E-04

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TWO-STAGE CMOS AMPLIFIER (GAIN FROM VDS)
*****
VDD 100 0 1.5
VSS 100 0 -1.5
M1 7 0 4 4 PMOS W=1500 L=10
M2 8 4 4 4 PMOS W=1500 L=10
M3 7 7 200 200 NMOS W=500 L=10
M4 8 7 200 200 NMOS W=500 L=10
M5 4 3 100 100 PMOS W=1500 L=10
M6 5 8 200 200 NMOS W=500 L=10
M7 5 3 100 100 PMOS W=1500 L=10
M8 3 3 200 200 PMOS W=1500 L=10
IRIAS 3 100 2000
* THE DC OFFSET IS ADJUSTED BY TRIAL AND ERROR
* TO GET THE OUTPUT TO ZERO.
VIL 5 3 4.00
VIO 4 3 0
+GAIN = LGAIN - 2LD -GD = 1 - 2(0.00) - 0.1 = 0.70 OM
+LAMBDA=(IDC/IDDC)/GAIN = 0.040/0.10 = 0.0004
.MODEL MOSFET LEVEL=1 KP=0.040 VTO=0.5 LAMBDA=0.0004
.MODEL PMOS PMOS LEVEL=1 KP=0.040 VTO=-0.5 LAMBDA=0.0004
.OPTIONS MESSAGE NONE
.MIXER OFF=0
.OPTIONS VTCOL=IN ANTIOL=IF BISTOL=00
.OFF
.OP VGS VDS
.END

**** OPERATING POINT INFORMATION TRNS= 27.000 TRNS= 27.000
NODE      +VOLTAGE      NODE      +VOLTAGE      NODE      +VOLTAGE
+0:1      = 0 0:3      = 3.000E-01  0:4      = 3.000E-01
+0:5      = 4.500E-06  0:6      = 0 0:7      =-7.500E-01
+0:8      =-7.500E-01  0:9      = 3.000E-04  0:100     = 1.500E-03
+0:100    =-1.500E-03

**** SMALL-SIGNAL TRANSFER CHARACTERISTICS
VGS/VDS = -3.640E-02
INPUT RESISTANCE AT VDS = 4.750E-04
OUTPUT RESISTANCE AT VGS = 4.750E-04

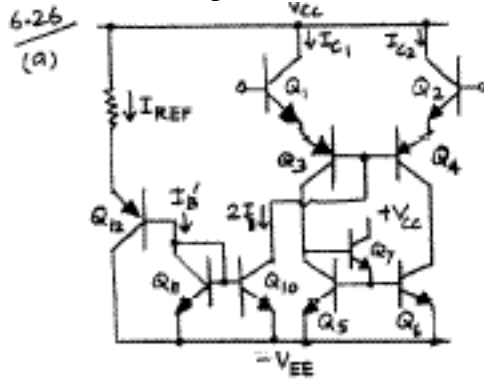
TWO-STAGE CMOS AMPLIFIER (GAIN FROM VGS)
*****
VDD 100 0 1.5
VSS 100 0 -1.5
M1 7 0 4 4 PMOS W=1500 L=10
M2 8 4 4 4 PMOS W=1500 L=10
M3 7 7 200 200 NMOS W=500 L=10
M4 8 7 200 200 NMOS W=500 L=10
M5 4 3 100 100 PMOS W=1500 L=10
M6 5 8 200 200 NMOS W=500 L=10
M7 5 3 100 100 PMOS W=1500 L=10
M8 3 3 200 200 PMOS W=1500 L=10
IRIAS 3 100 2000
* THE DC OFFSET IS ADJUSTED BY TRIAL AND ERROR
* TO GET THE OUTPUT TO ZERO.
VIL 5 3 4.00
VIO 4 3 0
+GAIN = LGAIN - 2LD -GD = 1 - 2(0.00) - 0.1 = 0.70 OM
+LAMBDA=(IDC/IDDC)/GAIN = 0.040/0.10 = 0.0004
.MODEL MOSFET LEVEL=1 KP=0.040 VTO=0.5 LAMBDA=0.0004
.MODEL PMOS PMOS LEVEL=1 KP=0.040 VTO=-0.5 LAMBDA=0.0004
.OPTIONS MESSAGE NONE
.MIXER OFF=0
.OPTIONS VTCOL=IN ANTIOL=IF BISTOL=00
.OFF
.OP VGS VDS
.END

**** OPERATING POINT INFORMATION TRNS= 27.000 TRNS= 27.000
NODE      +VOLTAGE      NODE      +VOLTAGE      NODE      +VOLTAGE
+0:1      = 0 0:3      = 3.000E-01  0:4      = 3.000E-01
+0:5      = 4.500E-06  0:6      = 0 0:7      =-7.500E-01
+0:8      =-7.500E-01  0:9      = 3.000E-04  0:100     = 1.500E-03
+0:100    =-1.500E-03

**** SMALL-SIGNAL TRANSFER CHARACTERISTICS
VGS/VDS = 3.640E-01
INPUT RESISTANCE AT VDS = 1.500E+00
OUTPUT RESISTANCE AT VGS = 4.750E-04

```

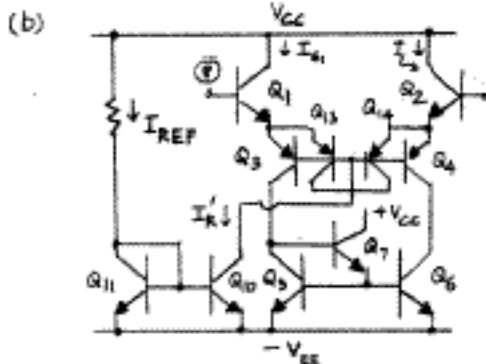
Problem 4 – (10 points)



$$I_{C1} = I_{C2} = 10 \mu A \quad \beta_{PNP} = 50$$

$$I_B = \frac{I_{C1}}{1 + \beta_{PNP}} \quad \therefore 2 I_B = 0.39 \mu A \approx I_B'$$

$$\therefore I_{REF} = (1 + \beta_{PNP}) I_B' = 20 \mu A$$



$$I_{C1} = I_{C2} = 10 \mu A$$

$$I_{E3} = I_{E13} = I_{E14} = I_{E4} \approx \frac{I_{C1}}{2} = 5 \mu A$$

$$I_{R'} = 2 |I_{C3}| + 4 |I_{B13}|$$

$$= 2 \left( \frac{5 \mu A}{1 + 50} \right) + 4 \cdot \left( \frac{5 \mu A}{1 + 50} \right)$$

$$= 10.2 \mu A = I_{REF}$$

T41 INPUT KERN SCHEM (A)

```

*****
VCC 100 0 10
VBE 200 0 -15
IREF 100 3 200
Q1 100 8 10 100
Q2 150 8 15 100
Q3 12 6 10 100
Q4 16 6 11 100
Q5 12 13 200 100
Q6 18 13 200 100
Q7 100 12 13 100
Q13 8 4 200 100
Q14 8 4 200 100
Q12 200 4 3 100
    
```

```

* WITH VIC = -12.6 V,
* VBE10 = VIC - VBE1 - (VBE1) - (-VBE)
* V = -12.6 - 0.6 - 0.6 + 15 = 1.2 V
* THIS IS ENOUGH TO OVERBIAS Q13 IN THE FORWARD-ACTIVE REGION.
V12 8 0 -12.6
V13 8 0 -12.6 AC 1
    
```

```

.MODEL NPN NPN BF=250 IS=1E-15
.MODEL PNP PNP BF=50 IS=1E-15
.OPTIONS NOVAE NOMOD
.LIBRARY DOUT=10
.OP
    
```

```

* VOLT IS USED TO MEASURE THE AC SHORT CIRCUIT OUTPUT
* CURRENT TO FIND GM.
* THE DC VALUE OF VOLT WAS GIVEN IN THE PROBLEM STATEMENT.
VOUT 10 200 1.4
    
```

```

.AC DEC 1 1 10
.PRINT AC IM(VOUT) IP(VOUT)
    
```

```

* THE TRANSCONDUCTANCE CAN ALSO BE MEASURED BY ELIMINATING
* THE VOLTAGE SOURCE CONNECTED AT THE OUTPUT AND THE
* AC ANALYSIS ABOVE, FINDING THE VOLTAGE GAIN AND OUTPUT
* TRANSCONDUCTANCE WITH A .VF STATEMENT AND OTHER DEVICES,
* AND CALCULATING GM = (VOLTAGE GAIN)/(OUTPUT RESISTANCE)
* THE RESULT IS GM = 1.736E+05.237E7 = 100E-6 A/V
*.VF V12(1) V12
.END
    
```

```

**** OPERATING POINT INFORMATION  TIME= 27.60E+00  TIME= 27.60E+00
NODE  +VOLTAGE  NODE  +VOLTAGE  NODE  +VOLTAGE
+0.3  --1.182E+01  0.14  --1.452E+01  0.0  --1.372E+01
+0.8  --1.280E+01  0.19  --1.280E+01  0.10  --1.308E+01
+0.11  --1.332E+01  0.12  --1.462E+01  0.13  --1.448E+01
+0.14  --1.348E+01  0.100  --1.508E+01  0.200  --1.508E+01
    
```

\*\*\* BIPOLAR JUNCTION TRANSISTORS

```

NODES
ELEMENT  Q:Q1  Q:Q2  Q:Q3  Q:Q4  Q:Q5
MODEL  0:0NPN  0:0NPN  0:0PNP  0:0PNP  0:0NPN
IB  3.945E-08  3.945E-08  -1.942E-07  -1.942E-07  3.945E-08
IC  9.462E-04  9.462E-04  -9.708E-04  -9.708E-04  9.708E-04
VBE  5.532E-01  5.532E-01  -5.708E-01  -5.708E-01  5.532E-01
VCE  3.812E+01  3.812E+01  -4.852E-01  -4.852E-01  9.812E-01
VBC  -2.742E-01  -2.742E-01  2.852E-01  2.852E-01  -4.282E-01
VE  -1.502E+01  -1.502E+01  1.772E-01  1.772E-01  3.412E-01
POWER  3.772E-04  3.772E-04  8.512E-05  8.512E-05  3.542E-04
MUTUAL  1.502E+01  1.502E+01  1.502E+01  4.982E-01  1.502E+01
GM  1.812E+04  1.812E+04  3.782E+04  3.782E+04  3.782E+04
BET  6.552E+05  6.552E+05  1.512E+05  1.512E+05  6.462E+05
BF  0.  0.  0.  0.  0.
RD  1.522E+15  1.522E+15  1.642E+14  1.642E+14  1.542E+15
BETAAC  1.502E+01  1.502E+01  1.502E+01  4.992E-01  1.502E+01
    
```

Problem 4 – Continued

```

**** AC ANALYSIS
      FREQ  I MAG  I PHASE
      VOLT  VOLT
1.0000E+00  1.077E-04  4.174E-21
1.0000E+01  1.077E-04  4.174E-21
    
```

```

**** AC ANALYSIS
      FREQ  I MAG  I PHASE
      VOLT  VOLT
1.0000E+00  1.077E-04  4.174E-21
1.0000E+01  1.077E-04  4.174E-21
    
```

TEL INPUT BIAS SOURCE (A)

```

****
VCC 100 0 10
VBE 100 0 -10
IBBP 100 0 10.100
Q1 100 0 10 NPN
Q2 100 0 11 NPN
Q3 10 0 10 PNP
Q4 10 0 11 PNP
Q5 10 10 100 NPN
Q6 10 10 10 NPN
Q7 100 10 10 NPN
Q10 0 4 100 NPN
Q11 0 4 100 NPN
* REMOVE Q13 FROM THE CIRCUIT.
* IT HAS ONLY BEING FOR BJT (A).
Q13 100 100 100 100 PNP
Q14 0 0 0 10 PNP
Q14 0 0 0 11 PNP
* WITH VCC = -10.0 V.
* VCE10 = VCC - VBE10 - [VBE10] = (-10V)
+ (-10.0 - 0.0 - 0.0 + 10 = 0.0 V
* Q10 IS BIAS TO OPERATE Q10 IN THE FORWARD-ACTIVE REGION.
V10 0 0 -10.0
V11 0 0 -10.0 AC 1
.MODEL NPN NPN BF=100 IS=1E-15
.MODEL PNP PNP BF=50 IS=1E-15
.OPTIONS BIPOLAR BIASED
.PRINTS OUT=10
.END
* VOLT IS USED TO MEASURE THE AC BIAS CIRCUIT OUTPUT
* CONVERT TO FIND gm.
* THE [G] VALUE OF BIAS HAS GIVEN IN THE PREVIOUS STATEMENT.
VOLT 10 100 1.0
.AC DEC 1 10
.PRINT AC (I(VOLT)) (V(VOLT))
* THE TRANSCONDUCTANCE CAN ALSO BE MEASURED BY ELIMINATING
* THE VOLTAGE SOURCE CONNECTED AT THE OUTPUT AND THE
* AC STATEMENT ABOVE. FINDING THE VOLTAGE GAIN AND OUTPUT
* RESISTANCE WITH A .TF STATEMENT AS SHOWN BELOW.
* ALSO CALCULATED gm = (VOLTAGE GAIN)/(OUTPUT RESISTANCE)
* THE RESULT IS gm = 1.0418A/V. TRANS = 1E-6 A/V
* THE TRANSCONDUCTANCE IS PRINTED HERE FORWARD
* TO THE TRANSCONDUCTANCE IS BJT (A) BIASING
* THE COLLECTOR CURRENT OF Q13 AND Q14 BIAS FLOW
* IN Q10 AND Q10 NOT CONTRIBUTING TO THE SIGNAL OUTPUT.
.TF V10
.END
    
```

```

**** OPERATING POINT INFORMATION
      TIME= 27.000 TEMP= 27.000
      NODE  VOLTAGE  NODE  VOLTAGE  NODE  VOLTAGE
+----+
+Q1  = 0.  0.0  =-1.444E+01  0.0  =-1.771E+01
+Q2  =-1.000E+01  0.0  =-2.300E+01  0.00  =-1.315E+00
+Q3  =-1.010E+01  0.12  =-2.400E+01  0.13  =-1.440E+01
+Q4  =-1.040E+01  0.100  =-2.500E+01  0.100  =-1.500E+01
    
```

\*\*\*\* BIPOLAR JUNCTION TRANSISTORS

```

**** BIPOLAR JUNCTION TRANSISTORS
      FREQ  I MAG  I PHASE
      VOLT  VOLT
1.0000E+00  1.077E-04  4.174E-21
1.0000E+01  1.077E-04  4.174E-21
    
```

```

**** AC ANALYSIS
      FREQ  I MAG  I PHASE
      VOLT  VOLT
1.0000E+00  1.077E-04  4.174E-21
1.0000E+01  1.077E-04  4.174E-21
    
```

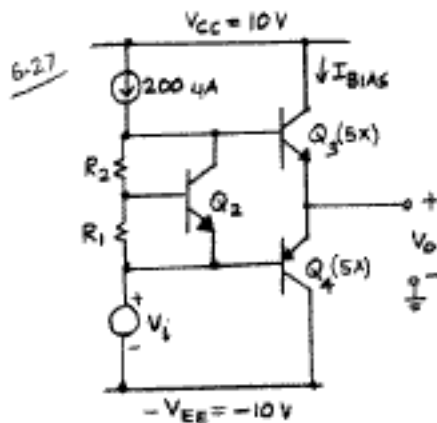
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**** AC ANALYSIS
      FREQ  I MAG  I PHASE
      VOLT  VOLT
1.0000E+00  1.077E-04  4.174E-21
1.0000E+01  1.077E-04  4.174E-21
    
```

```

**** AC ANALYSIS
      FREQ  I MAG  I PHASE
      VOLT  VOLT
1.0000E+00  1.077E-04  4.174E-21
1.0000E+01  1.077E-04  4.174E-21
    
```

## Problem 5 - (10 points)



Neglect current flow through  $R_1$  and  $R_2$  from  $200 \mu\text{A}$  source.

$$\therefore I_{C2} = 200 \mu\text{A}, V_{BE2} = V_T \ln \frac{I_{C2}}{I_{S2}}$$

$$\begin{aligned} V_{BE2} + V_{BE3} &= V_{BE2} + \frac{V_{BE2} \times R_2}{R_1} \\ &= \frac{V_T}{R_1} (R_1 + R_2) \ln \frac{I_{C2}}{I_{S2}} \\ &= V_T \ln \left( \frac{I_{C2} | I_{C4}|}{I_{S2} I_{S4}} \right) \end{aligned}$$

Areas of  $Q_3, Q_4$  are 5 times of  $Q_1$  and  $Q_2$ . Therefore,

$$I_{S1} = I_{S2} = 10^{-15} \text{A} = I_S$$

$$I_{S3} = I_{S4} = 5 \times 10^{-15} \text{A} = 5 I_S$$

$$V_T \ln \left( \frac{I_{BIAS}}{25 I_S^2} \right) = V_T \left( 1 + \frac{R_2}{R_1} \right) \ln \left( \frac{I_{C2}}{I_S} \right)$$

$$\begin{aligned} \therefore I_{BIAS} &= 5 I_S \left( \frac{I_{C2}}{I_S} \right)^{\frac{1}{2} \left( 1 + \frac{R_2}{R_1} \right)} \\ &= 5 (I_{C2})^{\frac{1}{2} \left( 1 + \frac{R_2}{R_1} \right)} (I_S)^{\frac{1}{2} \left( 1 - \frac{R_2}{R_1} \right)} \end{aligned} \rightarrow \textcircled{1}$$

$$\frac{R_2}{R_1} = \frac{2 \ln \left( \frac{I_{BIAS}}{5 I_S} \right)}{\ln \left( \frac{I_{C2}}{I_S} \right)} - 1$$

$$I_{BIAS} = 50 \mu\text{A}, I_S = 10^{-15} \text{A}, I_{C2} = 200 \mu\text{A}$$

$$\therefore \frac{R_2}{R_1} = 0.77$$

From  $\textcircled{1}$ , If we choose  $\frac{R_2}{R_1} = 1$

$$\text{then } I_{BIAS} = 5 (I_{C2})^{\frac{1}{2} \left( 1 + \frac{R_2}{R_1} \right)}$$

$$= 1000 \mu\text{A} = 1 \text{mA}$$

and  $I_{BIAS}$  is independent of temperature. In general, if  $\frac{R_2}{R_1} \neq 1$

then  $I_{BIAS}$  is dependent on temperature because  $I_S$  depends on temperature.



Problem 5 – Continued

```

T42 OUTPUT-STAGE BIAS SCHEME
* REPLACE TO CHECK BIAS CALCULATIONS
*****
VCC 100 0 10
VEE 100 0 -10
DEP 100 3 1000
Q1 3 4 3 NPN
Q2 100 3 6 NPN 5
Q4 100 3 4 PNP 5
R1 4 3 100K
R2 3 4 77K
V1 5 100 0.004
.MODEL NPN NPN BF=1000 IS=1E-15
.MODEL PNP PNP BF=1000 IS=1E-15
.OPTIONS MESSAGE=NONE
.WIDTH OPT=80
.OP
.END

```

```

**** OPERATING POINT INFORMATION  TIME= 27.000  TEMP= 27.000
NODE  +VOLTAGE  NODE  +VOLTAGE  NODE  +VOLTAGE
+0:3  = 7.748E-01  0:4  = 1.471E-01  0:5  =-5.800E-01
+0:6  = 9.112E-02  0:100 = 1.000E+01  0:100 =-1.000E+01

**** BIPOLAR JUNCTION TRANSISTORS
SUBCIR
ELEMENT 0:Q1 0:Q2 0:Q4
MODEL 0:NPV 0:NPV 0:PNP
IB 7.850E-07 3.110E-09 -2.933E-06
IC 1.813E-04 7.700E-05 -7.897E-09
VBE 7.877E-01 6.870E-01 -6.871E-01
VCE 1.374E+00 9.900E+00 -1.000E+01
BETA0 2.500E+02 2.500E+02 5.000E+01

```

```

T41 OUTPUT-STAGE BIAS SCHEME
* SET BY TO NOMINAL VALUES AND FOR TEMPERATURE SWEEP
*****
VCC 100 0 10
VEE 100 0 -10
DEP 100 3 2000
Q1 3 4 5 NPN
Q2 100 3 6 NPN 5
Q4 100 3 4 PNP 5
R1 4 3 100K
R2 3 4 77K
V1 5 100 0.404
.MODEL NPN NPN BF=210 IS=1E-15
.MODEL PNP PNP BF=90 IS=1E-15
.OPTIONS MESSAGE=NONE
.WIDTH OPT=80
.OP
TEMP -55 -0 -10 0 25 45 65 85 105 125
.END

```

```

**** OPERATING POINT INFORMATION  TIME= 27.000  TEMP= -55.000
NODE  +VOLTAGE  NODE  +VOLTAGE  NODE  +VOLTAGE
+0:3  = 8.397E-01  0:4  = 2.110E-01  0:5  =-5.800E-01
+0:6  = 1.497E-01  0:100 = 1.000E+01  0:100 =-1.000E+01

**** BIPOLAR JUNCTION TRANSISTORS
SUBCIR
ELEMENT 0:Q1 0:Q2 0:Q4
MODEL 0:NPV 0:NPV 0:PNP
IB 7.640E-07 1.101E-09 -6.403E-07
IC 1.910E-04 3.257E-05 -3.202E-09
VBE 8.000E-01 7.460E-01 -7.467E-01
VCE 1.451E+00 9.800E+00 -1.010E+01
BETA0 2.500E+02 2.500E+02 5.000E+01

```

```

**** OPERATING POINT INFORMATION  TIME= 27.000  TEMP= -25.000
NODE  +VOLTAGE  NODE  +VOLTAGE  NODE  +VOLTAGE
+0:3  = 8.375E-01  0:4  = 1.896E-01  0:5  =-5.800E-01
+0:6  = 1.100E-01  0:100 = 1.000E+01  0:100 =-1.000E+01

**** BIPOLAR JUNCTION TRANSISTORS
SUBCIR
ELEMENT 0:Q1 0:Q2 0:Q4
MODEL 0:NPV 0:NPV 0:PNP
IB 7.500E-07 2.000E-09 -1.007E-06
IC 1.910E-04 3.215E-05 -3.190E-09
VBE 7.900E-01 7.500E-01 -7.500E-01
VCE 1.450E+00 9.870E+00 -1.000E+01
BETA0 2.500E+02 2.500E+02 5.000E+01

```

```

**** OPERATING POINT INFORMATION  TIME= 27.000  TEMP= -15.000
NODE  +VOLTAGE  NODE  +VOLTAGE  NODE  +VOLTAGE
+0:3  = 7.748E-01  0:4  = 1.471E-01  0:5  =-5.800E-01
+0:6  = 9.112E-02  0:100 = 1.000E+01  0:100 =-1.000E+01

```

```

**** BIPOLAR JUNCTION TRANSISTORS
SUBCIR
ELEMENT 0:Q1 0:Q2 0:Q4
MODEL 0:NPV 0:NPV 0:PNP
IB 7.850E-07 3.110E-09 -2.933E-06
IC 1.813E-04 7.700E-05 -7.897E-09
VBE 7.877E-01 6.870E-01 -6.871E-01
VCE 1.374E+00 9.900E+00 -1.000E+01
BETA0 2.500E+02 2.500E+02 5.000E+01

```

```

**** OPERATING POINT INFORMATION  TIME= 27.000  TEMP= 5.000
NODE  +VOLTAGE  NODE  +VOLTAGE  NODE  +VOLTAGE
+0:3  = 7.180E-01  0:4  = 1.115E-01  0:5  =-5.800E-01
+0:6  = 8.125E-02  0:100 = 1.000E+01  0:100 =-1.000E+01

```

```

**** BIPOLAR JUNCTION TRANSISTORS
SUBCIR
ELEMENT 0:Q1 0:Q2 0:Q4
MODEL 0:NPV 0:NPV 0:PNP
IB 7.600E-07 4.400E-09 -2.160E-06
IC 1.920E-04 1.100E-04 -1.890E-04
VBE 7.090E-01 6.970E-01 -6.970E-01
VCE 1.310E+00 9.930E+00 -1.000E+01
BETA0 1.800E+02 2.500E+02 5.000E+01

```

```

**** OPERATING POINT INFORMATION  TIME= 27.000  TEMP= 25.000
NODE  +VOLTAGE  NODE  +VOLTAGE  NODE  +VOLTAGE
+0:3  = 6.580E-01  0:4  = 7.930E-02  0:5  =-5.800E-01
+0:6  = 2.207E-02  0:100 = 1.000E+01  0:100 =-1.000E+01

```

```

**** BIPOLAR JUNCTION TRANSISTORS
SUBCIR
ELEMENT 0:Q1 0:Q2 0:Q4
MODEL 0:NPV 0:NPV 0:PNP
IB 7.070E-07 5.940E-09 -2.920E-06
IC 1.920E-04 1.400E-04 -1.401E-04
VBE 6.750E-01 6.770E-01 -6.770E-01
VCE 1.260E+00 9.940E+00 -1.000E+01
BETA0 2.500E+02 2.500E+02 5.000E+01

```

```

**** OPERATING POINT INFORMATION  TIME= 27.000  TEMP= 45.000
NODE  +VOLTAGE  NODE  +VOLTAGE  NODE  +VOLTAGE
+0:3  = 5.970E-01  0:4  = 6.482E-02  0:5  =-5.800E-01
+0:6  = 9.720E-04  0:100 = 1.000E+01  0:100 =-1.000E+01

```

```

**** BIPOLAR JUNCTION TRANSISTORS
SUBCIR
ELEMENT 0:Q1 0:Q2 0:Q4
MODEL 0:NPV 0:NPV 0:PNP
IB 7.600E-07 7.700E-09 -1.810E-06
IC 1.920E-04 1.990E-04 -1.990E-04
VBE 6.400E-01 5.970E-01 -5.960E-01
VCE 1.280E+00 9.900E+00 -1.000E+01
BETA0 2.500E+02 2.500E+02 5.000E+01

```

```

**** OPERATING POINT INFORMATION  TIME= 27.000  TEMP= 65.000
NODE  +VOLTAGE  NODE  +VOLTAGE  NODE  +VOLTAGE
+0:3  = 5.300E-01  0:4  = 3.000E-02  0:5  =-5.800E-01
+0:6  =-9.821E-02  0:100 = 1.000E+01  0:100 =-1.000E+01

```

```

**** BIPOLAR JUNCTION TRANSISTORS
SUBCIR
ELEMENT 0:Q1 0:Q2 0:Q4
MODEL 0:NPV 0:NPV 0:PNP
IB 7.600E-07 9.700E-09 -4.810E-06
IC 1.920E-04 2.400E-04 -2.407E-04
VBE 6.000E-01 5.600E-01 -5.600E-01
VCE 1.120E+00 1.000E+01 -9.800E+00
BETA0 2.500E+02 2.500E+02 5.000E+01

```

Problem 5 – Continued

```

*** OPERATING POINT INFORMATION      TEMP= 27.000  TEMP= 27.000
NODE      +VOLTAGE      NODE      +VOLTAGE      NODE      +VOLTAGE
+Q:1      = 4.700E-01  Q:4      =-2.480E-02  Q:3      =-2.480E-01
+Q:6      =-6.127E-02  Q:100     = 2.000E-01  Q:100     =-1.000E-01
    
```

\*\*\* BIPOLAR JUNCTION TRANSISTORS

MODEL

```

ELEMENT  Q:Q1      Q:Q2      Q:Q4
MODEL    Q:PNP     Q:PNP     Q:PNP
IB       7.420E-07  1.200E-06  -2.812E-06
IC       1.422E-04  1.010E-04  -2.840E-04
VBE      5.710E-01  5.800E-01  -5.247E-01
VCE      1.000E+00  1.000E+01  -2.810E+00
BETA0    2.500E+02  2.500E+02  2.500E+02
    
```

```

*** OPERATING POINT INFORMATION      TEMP= 27.000  TEMP= 125.000
NODE      +VOLTAGE      NODE      +VOLTAGE      NODE      +VOLTAGE
+Q:3      = 4.210E-01  Q:4      =-2.970E-02  Q:5      =-2.970E-01
+Q:6      =-6.250E-02  Q:100     = 2.000E-01  Q:100     =-1.000E-01
    
```

\*\*\* BIPOLAR JUNCTION TRANSISTORS

MODEL

```

ELEMENT  Q:Q1      Q:Q2      Q:Q4
MODEL    Q:PNP     Q:PNP     Q:PNP
IB       1.487E-07  1.450E-06  -7.180E-06
IC       1.920E-04  1.420E-04  -3.270E-04
VBE      5.200E-01  5.000E-01  -5.010E-01
VCE      1.000E+00  1.000E+01  -3.200E+00
BETA0    2.500E+02  2.500E+02  2.500E+02
    
```

```

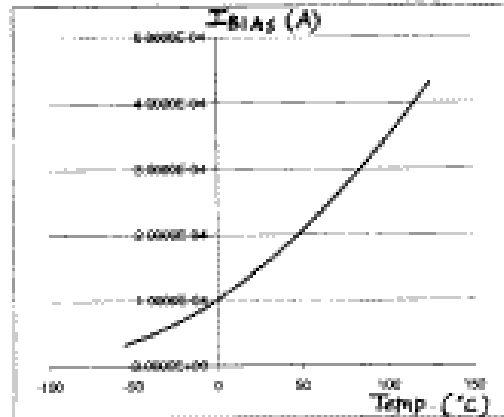
*** OPERATING POINT INFORMATION      TEMP= 27.000  TEMP= 125.000
NODE      +VOLTAGE      NODE      +VOLTAGE      NODE      +VOLTAGE
+Q:3      = 3.480E-01  Q:4      =-2.640E-02  Q:5      =-2.640E-01
+Q:6      =-1.242E-01  Q:100     = 2.000E+00  Q:100     =-1.000E-01
    
```

\*\*\* BIPOLAR JUNCTION TRANSISTORS

MODEL

```

ELEMENT  Q:Q1      Q:Q2      Q:Q4
MODEL    Q:PNP     Q:PNP     Q:PNP
IB       3.420E-07  3.720E-06  -8.400E-06
IC       1.920E-04  1.380E-04  -4.240E-04
VBE      5.000E-01  4.700E-01  -4.730E-01
VCE      2.442E-02  1.000E+01  -7.870E+00
BETA0    2.500E+02  2.500E+02  2.500E+02
    
```



TEMP (DEG C)	IC3 = IBIAS (A)	TEMP	IC4 = IBIAS (A)
-25	3.281E-06	25	1.970E-04
-10	3.225E-06	40	3.440E-04
+10	3.790E-06	55	3.214E-04
5	3.120E-04	100	3.430E-04
15	3.480E-04	125	4.290E-04