

Homework Assignment No. 8 - Solutions

Problem 1 - (10 points)

This problem deals with the op amp shown in Fig. P6.5-15. All device lengths are $1\mu\text{m}$, the slew rate is $\pm 10\text{V}/\mu\text{s}$, the GB is 10MHz , the maximum output voltage is $+2\text{V}$, the minimum output voltage is -2V , and the input common mode range is from -1V to $+2\text{V}$.

Design all W values of all transistors in this op amp. Your design must meet or

exceed the specifications. When calculating the maximum or minimum output voltages, divide the voltage drop across series transistors equally. Ignore bulk effects in this problem. When you have completed your design, find the value of the small signal differential voltage gain, $A_{vd} = v_{out}/v_{id}$, where $v_{id} = v_1 - v_2$ and the small signal output resistance, R_{out} .

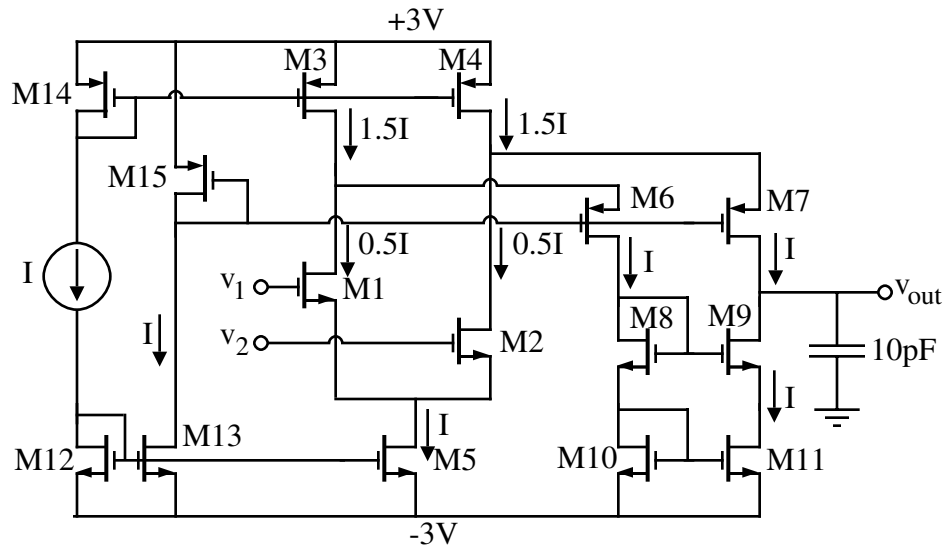


Figure P6.5-15

Solution

- 1.) The slew rate will specify I . $\therefore I = C \cdot SR = 10^{-11} \cdot 10^7 = 10^{-4} = 100\mu\text{A}$.
- 2.) Use GB to define W_1 and W_2 .

$$GB = \frac{g_{m1}}{C} \rightarrow g_{m1} = GB \cdot C = 2\pi \times 10^7 \cdot 10^{-11} = 628\mu\text{S}$$

$$\therefore W_1 = \frac{g_{m1}^2}{2K_N(0.5I)} = \frac{(628)^2}{2 \cdot 110 \cdot 50} = 35.85 \Rightarrow \underline{\underline{W_1 = W_2 = 36\mu\text{m}}}$$

- 3.) Design W_{15} to give $V_T + 2V_{ON}$ bias for M6 and M7. $V_{ON} = 0.5\text{V}$ will meet the desired maximum output voltage specification. Therefore,

$$V_{SG15} = V_{ON15} + |V_T| = 2(0.5\text{V}) + |V_T| \rightarrow V_{ON15} = 1\text{V} = \sqrt{\frac{2I}{K_P W_{15}}}$$

$$\therefore W_{15} = \frac{2I}{K_P V_{ON15}^2} = \frac{2 \cdot 100}{50 \cdot 1^2} = 4\mu\text{m} \Rightarrow \underline{\underline{W_{15} = 4\mu\text{m}}}$$

- 4.) Design W_3 , W_4 , W_6 and W_7 to have a saturation voltage of 0.5V with $1.5I$ current.

$$W_3 = W_4 = W_6 = W_7 = \frac{2(1.5I)}{K_P V_{ON}^2} = \frac{2 \cdot 150}{50 \cdot 0.5^2} = 24\mu\text{m} \Rightarrow \underline{\underline{W_3 = W_4 = W_6 = W_7 = 24\mu\text{m}}}$$

Problem 6.5-15 – Continued

5.) Next design W_8, W_9, W_{10} and W_{11} to meet the minimum output voltage specification. Note that we have not taken advantage of smallest minimum output voltage because a normal cascode current mirror is used which has a minimum voltage across it of $V_T + 2V_{ON}$. Therefore, setting $V_T + 2V_{ON} = 1V$ gives $V_{ON} = 0.15V$. Using worst case current, we choose $1.5I$. Therefore,

$$W_8 = W_9 = W_{10} = W_{11} = \frac{2(1.5I)}{K_N V_{ON}^2} = \frac{2 \cdot 150}{110 \cdot 0.15^2} = 121 \mu\text{m} \Rightarrow \underline{\underline{W_8 = W_9 = W_{10} = W_{11} = 121 \mu\text{m}}}$$

6.) Check the maximum ICM voltage.

$$V_{ic}(\text{max}) = V_{DD} + V_{SD3}(\text{sat}) + V_{TN} = 3V - 0.5 + 0.7 = 3.2V \text{ which exceeds spec.}$$

7.) Use the minimum ICM voltage to design W_5 .

$$V_{ic}(\text{min}) = V_{SS} + V_{DS5}(\text{sat}) + V_{GS1} = -3 + V_{DS5}(\text{sat}) + \left(\sqrt{\frac{2 \cdot 50}{110 \cdot 36}} + 0.7 \right) = -1V$$

$$\therefore V_{DS5}(\text{sat}) = 1.141 \rightarrow W_5 = \frac{2I}{K_N V_{DS5}(\text{sat})^2} = 1.39 \mu\text{m} = 1.4 \mu\text{m}$$

Also, let $W_{12} = W_{13} = W_5 \Rightarrow \underline{\underline{W_{12} = W_{13} = W_5 = 1.4 \mu\text{m}}}$

8.) W_{14} is designed as

$$W_{14} = W_3 \frac{I_{14}}{I_3} = 24 \mu\text{m} \frac{I}{1.5I} = 16 \mu\text{m} \Rightarrow \underline{\underline{W_{14} = 16 \mu\text{m}}}$$

Now, calculate the op amp small-signal performance.

$$R_{out} \approx r_{ds11} g_{m9} r_{ds9} \| g_{m7} r_{ds7} (r_{ds2} \| r_{ds4})$$

$$g_{m9} = \sqrt{2K_N I \cdot W_9} = 1632 \mu\text{S}, \quad r_{ds9} = r_{ds11} = \frac{25V}{100 \mu\text{A}} = 0.25 \text{M}\Omega,$$

$$g_{m7} = \sqrt{2K_P I \cdot W_7} = 490 \mu\text{S}, \quad r_{ds7} = \frac{20V}{100 \mu\text{A}} = 0.2 \text{M}\Omega, \quad r_{d2} = \frac{25V}{50 \mu\text{A}} = 0.5 \text{M}\Omega$$

$$r_{ds4} = \frac{20V}{150 \mu\text{A}} = 0.1333 \text{M}\Omega \quad \therefore \underline{\underline{R_{out} \approx 102 \text{M}\Omega \| 10.31 \text{M}\Omega = 9.3682 \text{M}\Omega}}$$

$$A_{vd} = \left(\frac{2+k}{2+2k} \right) g_{m1} R_{out}, \quad k = \frac{102 \text{M}\Omega}{(r_{ds2} \| r_{ds4}) g_{m7} r_{ds7}} = 9.888, \quad g_{m1} = \sqrt{K_N I \cdot W_1} = 629 \mu\text{S}$$

$$\therefore A_{vd} = (0.5459)(629 \mu\text{S})(9.3682 \text{M}\Omega) = 3,217 \text{V/V} \Rightarrow \underline{\underline{A_{vd} = 3,217 \text{V/V}}}$$

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**** OPERATING POINT INFORMATION      TNOM= 27.000  TEMP= 85.000
  NODE      =VOLTAGE      NODE      =VOLTAGE      NODE      =VOLTAGE
+0:3        = 4.739E-01  0:4        =-2.498E-02  0:5        =-5.960E-01
+0:6        =-6.127E-02  0:100       = 1.000E+01  0:200       =-1.000E+01
**** BIPOLAR JUNCTION TRANSISTORS
SUBCKT
ELEMENT 0:Q2      0:Q3      0:Q4
MODEL  0:NPN      0:NPN      0:PNP
IB      7.693E-07  1.205E-06  -5.933E-06
IC      1.923E-04  3.014E-04  -2.966E-04
VBE     5.710E-01  5.352E-01  -5.347E-01
VCE     1.069E+00  1.006E+01  -9.938E+00
BETAD   2.500E+02  2.500E+02  5.000E+01
    
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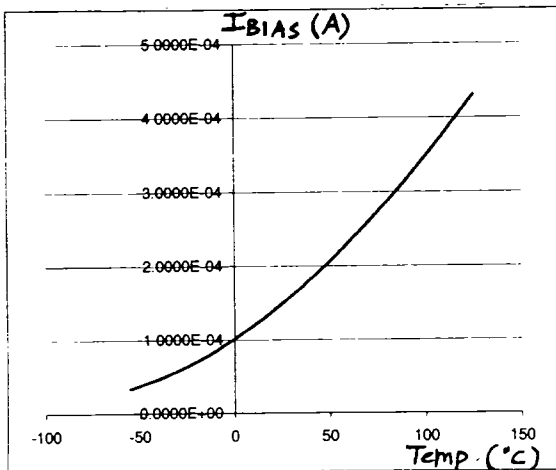
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**** OPERATING POINT INFORMATION      TNOM= 27.000  TEMP= 105.000
  NODE      =VOLTAGE      NODE      =VOLTAGE      NODE      =VOLTAGE
+0:3        = 4.113E-01  0:4        =-6.037E-02  0:5        =-5.960E-01
+0:6        =-9.259E-02  0:100       = 1.000E+01  0:200       =-1.000E+01
**** BIPOLAR JUNCTION TRANSISTORS
SUBCKT
ELEMENT 0:Q2      0:Q3      0:Q4
MODEL  0:NPN      0:NPN      0:PNP
IB      7.697E-07  1.454E-06  -7.158E-06
IC      1.924E-04  3.636E-04  -3.579E-04
VBE     5.356E-01  5.039E-01  -5.034E-01
VCE     1.007E+00  1.009E+01  -9.907E+00
BETAD   2.500E+02  2.500E+02  5.000E+01
    
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**** OPERATING POINT INFORMATION      TNOM= 27.000  TEMP= 125.000
  NODE      =VOLTAGE      NODE      =VOLTAGE      NODE      =VOLTAGE
+0:3        = 3.482E-01  0:4        =-9.604E-02  0:5        =-5.960E-01
+0:6        =-1.242E-01  0:100       = 1.000E+01  0:200       =-1.000E+01
**** BIPOLAR JUNCTION TRANSISTORS
SUBCKT
ELEMENT 0:Q2      0:Q3      0:Q4
MODEL  0:NPN      0:NPN      0:PNP
IB      7.699E-07  1.723E-06  -8.480E-06
IC      1.925E-04  4.308E-04  -4.240E-04
VBE     5.000E-01  4.724E-01  -4.718E-01
VCE     9.442E-01  1.012E+01  -9.875E+00
BETAD   2.500E+02  2.500E+02  5.000E+01
    
```

TEMP (DEG C)	IC3 = IBIAS (A)	TEMP	IC3 = IBIAS (A)
-55	3.253E-05	45	1.935E-04
-35	5.215E-05	65	2.446E-04
-15	7.790E-05	85	3.014E-04
5	1.100E-04	105	3.636E-04
25	1.486E-04	125	4.308E-04



6-28

If the bias current level of 741 input stage is doubled, then from (6.134), $G_{m1} = \frac{1}{2.7 \text{ k}\Omega}$

From (6.138),

$$R_{o1} = R_{out|Q4} \parallel R_{out|Q6} = 2 r_{o4} \parallel r_{o6} (1 + g_{m6} (1 \text{ k}\Omega))$$

Using $\eta_{npn} = 2 \times 10^{-4}$, $\eta_{pnp} = 5 \times 10^{-4}$

and $|I_c| = 19.4 \text{ A}$, we have

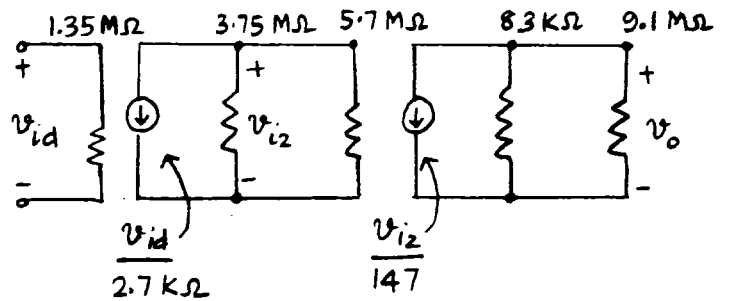
$$r_{o4} = \frac{1}{\eta g_m} = \frac{10^4}{5} \frac{26}{19 \times 10^{-3}} = 2.74 \text{ M}\Omega$$

$$r_{o6} = \frac{10^4}{2} \frac{26}{19 \times 10^{-3}} = 6.84 \text{ M}\Omega$$

$$g_{m6} \times 1 \text{ k}\Omega = 0.73$$

$$\therefore R_{o1} = (5.48) \parallel (6.84 \times 1.73) \text{ M}\Omega = 3.75 \text{ M}\Omega$$

741 equivalent



$$3.75 \parallel 5.7 = 2.26 \text{ M}\Omega ; 83 \text{ k}\Omega \parallel 9.1 \text{ M}\Omega = 82 \text{ k}\Omega$$

$$A_v = \frac{2260}{2.7} \cdot \frac{82}{0.147} = 838 \times 558 = 468,000$$

6.29

If the 100Ω emitter resistor of Q_{17} is removed, then in (6.142) we have,

$$R_{eq1} = r_{\pi 17} \pm \frac{\beta}{g_m} = 250 \times \frac{26}{0.55} = 11.8 \text{ k}\Omega$$

$$\begin{aligned} R_{i2} &= r_{\pi 16} + (1 + \beta_0)(r_{\pi 17} \parallel 50 \text{ k}\Omega) \\ &= 406 \text{ k}\Omega + 251 \times 9.55 \text{ k}\Omega \\ &= 2.8 \text{ M}\Omega \end{aligned}$$

From (6.146)

$$G_{m2} \approx g_{m17} = \frac{0.55}{26} = \frac{1}{47.3 \Omega}$$

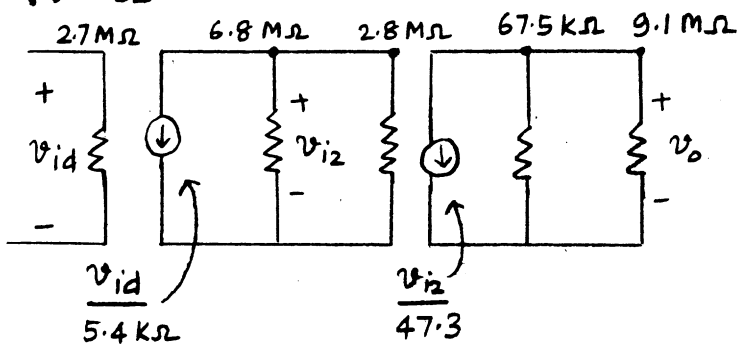
From (6.147)

$$R_{o2} = r_{o13\beta} \parallel r_{o17}$$

$$r_{o13\beta} = \frac{1}{\eta g_m} = \frac{10^4}{5} \frac{26}{0.55} = 94.5 \text{ k}\Omega$$

$$r_{o17} = \frac{1}{\eta g_m} = \frac{10^4}{2} \frac{26}{0.55} = 236 \text{ k}\Omega$$

$$\therefore R_{o2} = 67.5 \text{ k}\Omega$$



$$\begin{aligned} A_v &= \frac{1980}{5.4} \times \frac{67}{0.047} \quad 67.5 \text{ k}\Omega \parallel 9.1 \text{ M}\Omega = 67 \text{ k}\Omega \\ &= 523,000 \end{aligned}$$

6.30

Minimum CM input voltage:

The circuit ceases to function correctly when Q_3 and Q_4 saturate.

Q_3 and Q_4 operate in the F.A.R. when,

$$V_{EC3} > V_{CE(sat)}$$

$$V_{E3} = V_{IC} - V_{BE1} \quad \text{neglect}$$

$$V_{C3} = -V_{EE} + V_{BE5} + V_{BE7} + I_{C3}(1 \text{ k}\Omega)$$

$$V_{EC3} = V_{IC} - V_{BE1} - (-V_{EE}) - V_{BE5} - V_{BE7} > V_{CE(sat)}$$

$$V_{IC} > -V_{EE} + V_{BE1} + V_{BE5} + V_{BE7} + V_{CE(sat)}$$

Maximum CM input voltage:

Q_1 and Q_2 operate in the F.A.R. when

$$V_{CE1} > V_{CE(sat)}$$

$$V_{C1} = V_{CC} - |V_{BE8}|$$

$$V_{E1} = V_{IC} - V_{BE1}$$

$$V_{CE1} = V_{CC} - |V_{BE8}| - V_{IC} + V_{BE1} > V_{CE(sat)}$$

Assume $V_{BE1} = |V_{BE8}|$

$$\text{Then } V_{IC} < V_{CC} - V_{CE(sat)}$$

741 AS A VOLTAGE FOLLOWER

* POWER SUPPLIES
VCC 100 0 15
VEE 200 0 -15

* INPUT STAGE
Q1 7 8 10 NPN
Q2 7 9 11 NPN
Q3 12 6 10 PNP
Q4 16 6 11 PNP
Q5 12 13 14 NPN
Q6 16 13 15 NPN
Q7 100 12 13 NPN
Q8 7 7 100 PNP
Q9 6 7 100 PNP
Q10 6 4 5 NPN
Q11 4 4 200 NPN
Q12 3 3 100 PNP
R1 14 200 1K
R2 15 200 1K
R3 13 200 50K
R5 3 4 39K
R4 5 200 5K

* DARLINGTON GAIN STAGE
Q13B 19 3 100 PNPB
Q16 100 16 17 NPN
Q17 19 17 18 NPN
R8 18 200 100
R9 17 200 50K

* OUTPUT STAGE
Q13A 20 3 100 PNPB
Q14 100 20 25 NPN 3
Q18 20 21 22 NPN
Q19 20 20 21 NPN
Q20 200 22 23 PNP 3
Q23 200 19 22 PNP
R6 25 9 27
R7 23 9 22
R10 21 22 40K

V11 8 0 0
.MODEL NPN NPN BF=250 IS=5E-15 VAF=130
.MODEL PNP PNP BF=50 IS=2E-15 VAF=50
.MODEL PNPB PNPB BF=50 IS=0.5E-15 VAF=50
.MODEL PNPB PNPB BF=50 IS=1.5E-15 VAF=50
.OPTIONS NOPAGE NOMOD
.WIDTH OUT=80
.OP
.DC V11 -15 15 0.5

* ASSUMING VCE(SAT) = 0.2 V AND VBE(ON) = 0.7 V,
* THE HAND CALCULATIONS PREDICT A COMMON-MODE RANGE OF
* -12.7 V < VIC < 14.8 V
* IN THE VOLTAGE-FOLLOWER CONFIGURATION, VO = VI = VIC
* AS LONG AS THE AMPLIFIER IS WORKING CORRECTLY.
* THE RESULTS OF THIS SIMULATION SHOW THAT
* VO = VI FOR THE FOLLOWING RANGE:
* -13 V < VI < 14.5 V
* THEREFORE, THIS SIMULATION SHOWS THAT THE
* COMMON MODE INPUT RANGE IS:
* -13 V < (VO = VI = VIC) < 14.5 V
* WHICH IS CLOSE TO THE RESULT
* PREDICTED BY HAND CALCULATIONS.

.PLOT DC V(9)
.END

***** DC TRANSFER CURVES THOM= 27.000 TEMP= 27.000

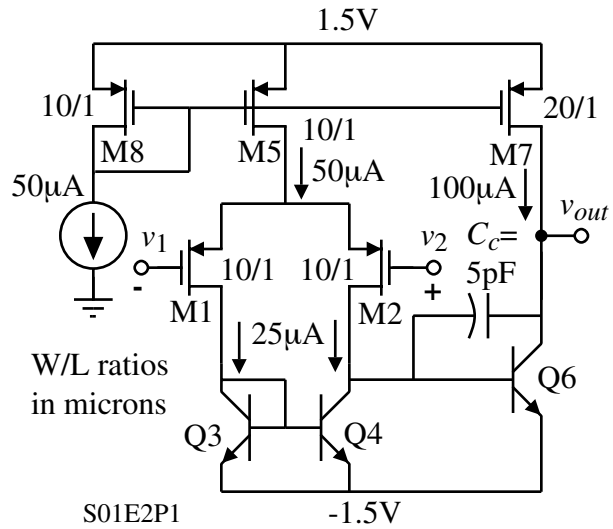
VOLT	V(9)					
(A)		-2.000E+01	-1.000E+01	0.	1.000E+01	2.000E+01
-1.500E+01	-1.31E+01		A			
-1.450E+01	-1.31E+01		A			
-1.400E+01	-1.31E+01		A			
-1.350E+01	-1.31E+01		A			
-1.300E+01	-1.30E+01		A			
-1.250E+01	-1.25E+01		A			
-1.200E+01	-1.20E+01		A			
-1.150E+01	-1.15E+01		A			
-1.100E+01	-1.10E+01		A			
-1.050E+01	-1.05E+01		A			
-1.000E+01	-9.99E+00		A			
-9.500E+00	-9.50E+00		A			
-9.000E+00	-9.00E+00		A			
-8.500E+00	-8.50E+00		A			
-8.000E+00	-8.00E+00		A			
-7.500E+00	-7.50E+00		A			
-7.000E+00	-7.00E+00		A			
-6.500E+00	-6.50E+00		A			
-6.000E+00	-6.00E+00		A			
-5.500E+00	-5.50E+00		A			
-5.000E+00	-5.00E+00		A			
-4.500E+00	-4.50E+00		A			
-4.000E+00	-4.00E+00		A			
-3.500E+00	-3.50E+00		A			
-3.000E+00	-3.00E+00		A			
-2.500E+00	-2.50E+00		A			
-2.000E+00	-2.00E+00		A			
-1.500E+00	-1.50E+00		A			
-1.000E+00	-1.00E+00		A			
-5.000E-01	-5.00E-01		A			
0.	2.74E-04		A			
5.000E-01	5.00E-01		A			
1.000E+00	1.00E+00		A			
1.500E+00	1.50E+00		A			
2.000E+00	2.00E+00		A			
2.500E+00	2.50E+00		A			
3.000E+00	3.00E+00		A			
3.500E+00	3.50E+00		A			
4.000E+00	4.00E+00		A			
4.500E+00	4.50E+00		A			
5.000E+00	5.00E+00		A			
5.500E+00	5.50E+00		A			
6.000E+00	6.00E+00		A			
6.500E+00	6.50E+00		A			
7.000E+00	7.00E+00		A			
7.500E+00	7.50E+00		A			
8.000E+00	8.00E+00		A			
8.500E+00	8.50E+00		A			
9.000E+00	9.00E+00		A			
9.500E+00	9.50E+00		A			
1.000E+01	1.00E+01		A			
1.050E+01	1.05E+01		A			
1.100E+01	1.10E+01		A			
1.150E+01	1.15E+01		A			
1.200E+01	1.20E+01		A			
1.250E+01	1.25E+01		A			
1.300E+01	1.30E+01		A			
1.350E+01	1.35E+01		A			
1.400E+01	1.40E+01		A			
1.450E+01	1.45E+01		A			
1.500E+01	1.46E+01		A			

**** OPERATING POINT INFORMATION THOM= 27.000 TEMP= 27.000

NODE	=VOLTAGE	NODE	=VOLTAGE	NODE	=VOLTAGE
+0:3	= 1.431E+01 0:4		= -1.433E+01 0:5		= -1.490E+01
+0:6	= -1.107E+00 0:7		= 1.441E+01 0:8		= 0.
+0:9	= 2.744E-04 0:10		= -5.439E-01 0:11		= -5.437E-01
+0:12	= -1.389E+01 0:13		= -1.444E+01 0:14		= -1.499E+01
+0:15	= -1.499E+01 0:16		= -1.370E+01 0:17		= -1.426E+01
+0:18	= -1.493E+01 0:19		= -1.260E+00 0:20		= 5.904E-01
+0:21	= 2.345E-02 0:22		= -6.088E-01 0:23		= -2.361E-03
+0:25	= 3.509E-03 0:100		= 1.500E+01 0:200		= -1.500E+01

Problem 5 – (10 points)

A two-stage, BiCMOS op amp is shown. For the PMOS transistors, the model parameters are $K_P' = 50\mu\text{A}/\text{V}^2$, $V_{TP} = -0.7\text{V}$ and $\lambda_P = 0.05\text{V}^{-1}$. For the NPN BJTs, the model parameters are $\beta_F = 100$, $V_{CE}(\text{sat}) = 0.2\text{V}$, $V_A = 25\text{V}$, $V_t = 26\text{mV}$, $I_s = 10\text{fA}$ and $n=1$. (a.) Identify which input is positive and which input is negative. (b.) Find the numerical values of differential voltage gain magnitude, $|A_v(0)|$, GB (in Hertz), the slew rate, SR , and the location of the RHP zero. (c.) Find the numerical value of the maximum and minimum input common mode voltages.

**Solution**

(a.) The plus and minus signs on the schematic show which input is positive and negative.

(b.) The differential voltage gain, $A_v(0)$, is given as

$$A_v(0) = \frac{g_{m1}}{g_{ds2} + g_{o4} + g_{\pi6}} \cdot \frac{g_{m6}}{g_{ds7} + g_{o6}} \quad g_{m1} = g_{m2} = \sqrt{2 \cdot 50 \cdot 25 \cdot 10} = 158.1\mu\text{S}$$

$$r_{ds2} = \frac{1}{\lambda_P I_D} = \frac{20}{25\mu\text{A}} = 0.8\text{M}\Omega, \quad r_{o4} = \frac{V_A}{I_C} = \frac{25\text{V}}{25\mu\text{A}} = 1\text{M}\Omega, \quad g_{m6} = \frac{I_C}{V_t} = \frac{100\mu\text{A}}{26\text{mV}} = 3846\mu\text{S}$$

$$r_{\pi6} = \frac{\beta_F}{g_{m6}} = 26\text{k}\Omega, \quad r_{ds7} = \frac{1}{\lambda_P I_D} = \frac{20}{100\mu\text{A}} = 0.2\text{M}\Omega \quad \text{and} \quad r_{o6} = \frac{V_A}{I_C} = \frac{25\text{V}}{100\mu\text{A}} = 0.25\text{M}\Omega$$

$$\therefore |A_v(0)| = [158.1(0.8 \parallel 1 \parallel 0.026)][3846(0.2 \parallel 0.25)] = 3.888 \cdot 427.36 = \underline{\underline{1,659.6\text{V/V}}}$$

$$GB = \frac{g_{m1}}{C_c} = \frac{158.1\mu\text{S}}{5\text{pF}} = 31.62 \times 10^6 \text{ rads/sec} \rightarrow \underline{\underline{GB = 5.0325\text{MHz}}}$$

$$SR = \frac{50\mu\text{A}}{5\text{pF}} = \underline{\underline{10\text{V}/\mu\text{s}}}$$

$$\text{RHP zero} = \frac{g_{m6}}{C_c} = \frac{3.846\text{mS}}{5\text{pF}} = \underline{\underline{769.24 \times 10^6 \text{ rads/sec. (122MHz)}}}$$

(c.) The maximum input common mode voltage is given as

$$v_{icm}^+ = V_{CC} - V_{DS5}(\text{sat}) - V_{SG1} = 1.5 - \sqrt{\frac{2 \cdot 50}{50 \cdot 10}} - 0.7 - \sqrt{\frac{2 \cdot 25}{50 \cdot 10}} = 0.8 - 0.447 - 0.316 =$$

$$\therefore v_{icm}^+ = \underline{\underline{0.0367\text{V}}}$$

$$v_{icm}^- = -1.5 + V_{BE3} - V_{T1} = -1.5 + V_t \ln\left(\frac{25\mu\text{A}}{10\text{fA}}\right) - 0.7 = -2.2 + 0.5626 = \underline{\underline{-1.6374\text{V}}}$$