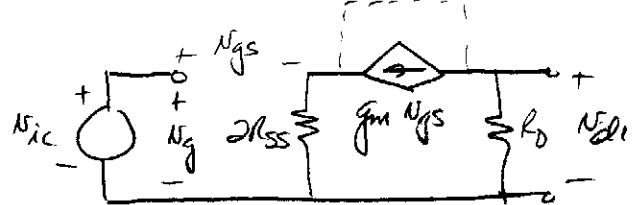
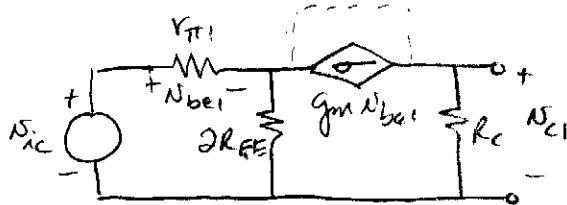
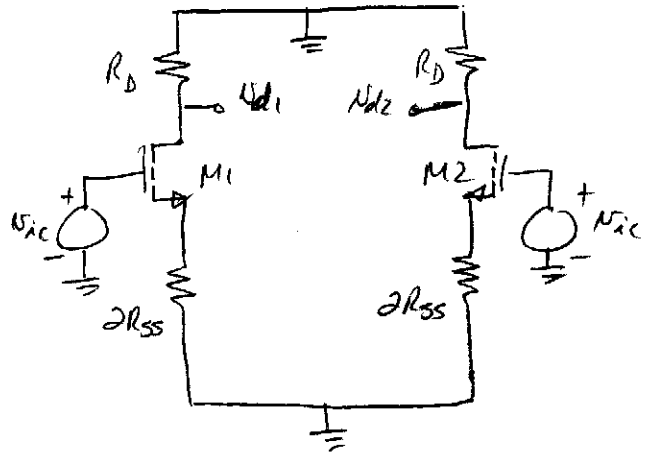
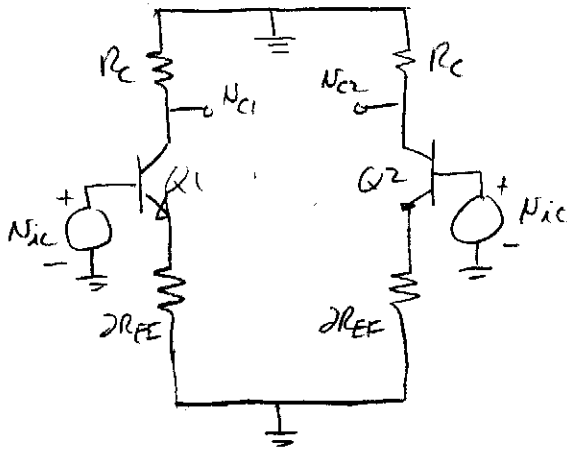


LECTURE 24

Common-mode Half Circuit -



$$A_{cd} = \frac{N_{c1}}{N_{ic}} = \left( \frac{N_{c1}}{N_{be1}} \right) \left( \frac{N_{be1}}{N_{ic}} \right)$$

$$A_{cd} = \frac{N_{d1}}{N_{ic}} = \left( \frac{N_{d1}}{N_{gs}} \right) \left( \frac{N_{gs}}{N_{ic}} \right)$$

$$N_{be1} = N_{b1} - N_{e1}$$

$$N_{gs} = N_g - N_s = N_{ic} - g_m 2R_{SS} N_{gs}$$

$$= N_{ic} - 2R_{EE} \left( \frac{1}{r_{\pi 1}} + g_{m1} \right) N_{be1}$$

$$\frac{N_{gs}}{N_{ic}} = \frac{1}{1 + 2g_m r_{SS}}$$

$$\frac{N_{be}}{N_{ic}} = \frac{1}{1 + \frac{2R_{EE}(1+\beta_1)}{r_{\pi 1}}}$$

$$\therefore A_{cd} = \frac{g_m R_D}{1 + 2g_m r_{SS}}$$

$$\therefore \frac{N_{c1}}{N_{ic}} = \frac{-g_{m1} R_C}{1 + \frac{2R_{EE}(1+\beta_1)}{r_{\pi 1}}}$$

$$R_{ic} = \infty$$

$$= \frac{-\beta_1 R_C}{r_{\pi 1} + (1+\beta_1) 2R_{EE}}$$

$$CMRR = \frac{|A_{cd}|}{|A_{ic}|} = \frac{\frac{g_m R_D}{2}}{\frac{g_m R_D}{1 + 2g_m r_{SS}}}$$

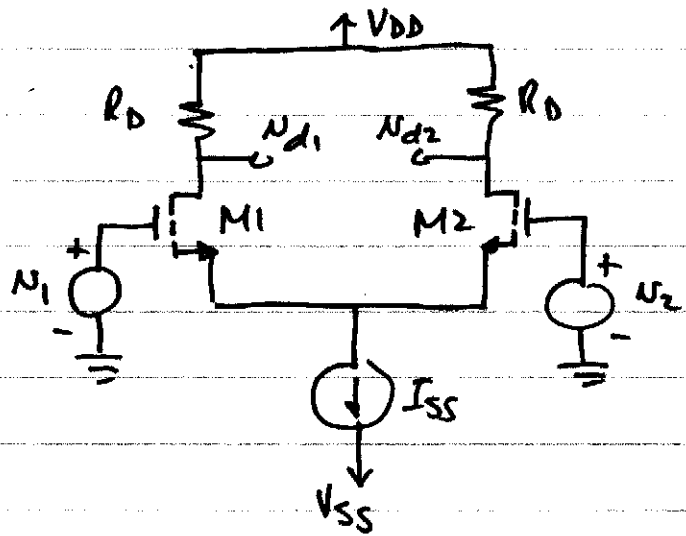
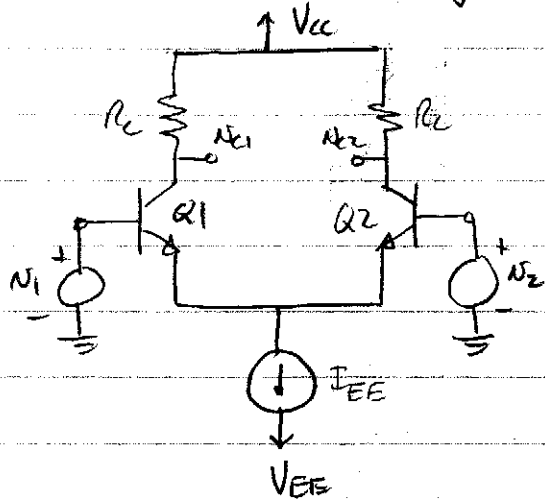
$$R_{ic} = \frac{N_{ic}}{2i_b} = \frac{r_{\pi 1} + (1+\beta_1) 2R_{EE}}{2}$$

$$\approx \underline{\underline{g_m r_{SS}}}$$

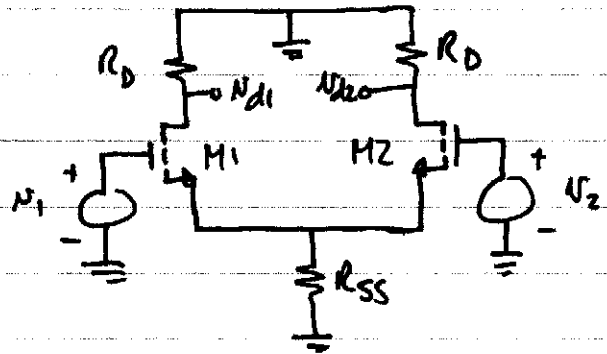
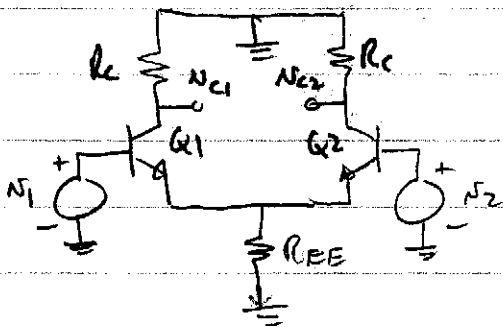
$$\therefore CMRR = \frac{|A_{cd}|}{|A_{ic}|} = \frac{g_m R_D}{2\beta_1 R_C} \left( \frac{r_{\pi 1} + (1+\beta_1) 2R_{EE}}{2} \right)$$

$$= 1 + \frac{(1+\beta_1) 2R_{EE}}{r_{\pi 1}} \approx g_m R_{EE}$$

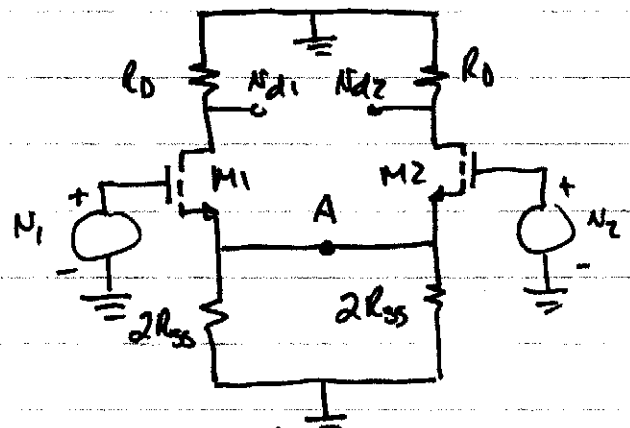
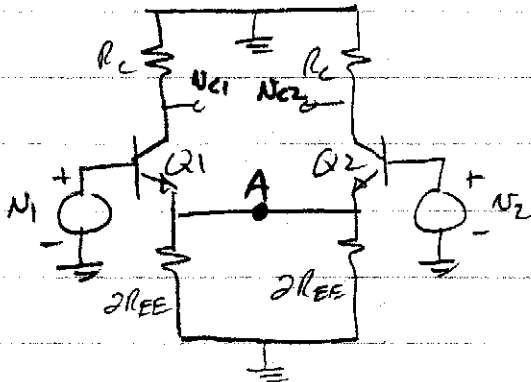
## Current sink biasing of Differential Amplifiers



AC circuit -



OV



Now, for differential mode analysis ( $N_{id}$ ) ground A and repeat the previous analysis for common mode analysis ( $N_{ic}$ ) cut the connection at A and repeat the previous analysis for half-circuits.