

### Homework Assignment No. 10 - Solutions

Problem 1 - (10 points)

Problem 8.13 of GHLM

Bias

$$I_{C1} + I_{C2} = \frac{5.3}{5} = 1.06 \text{ mA}$$

$$I_{C1} = \frac{V_{BE3}}{1.25} = \frac{0.7}{1.25} = 0.56 \text{ mA}$$

$$\therefore I_{C2} = 0.5 \text{ mA}$$

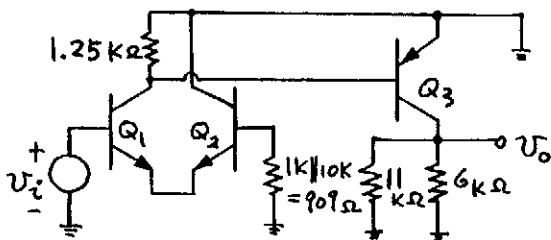
$$I_{C3} = \frac{6V}{6k\Omega} = 1 \text{ mA for } V_o|_{dc} = 0$$

Assume  $I_{C1} = I_{C2} = 0.53 \text{ mA}$

$$\text{Then } r_{\pi 1} = r_{\pi 2} = \frac{200 \times 26}{0.53} = 9.81 \text{ k}\Omega$$

$$r_{\pi 3} = 2.6 \text{ k}\Omega$$

Basic amplifier



$$\frac{V_o}{V_i} = \frac{g_{m1}}{1 + g_{m1} R_{E1}} R_1 g_{m3} R_2$$

$$R_{E1} = \frac{1}{g_{m2}} + \frac{909}{\beta_2} = \frac{26}{0.53} + \frac{909}{200} = 54 \Omega$$

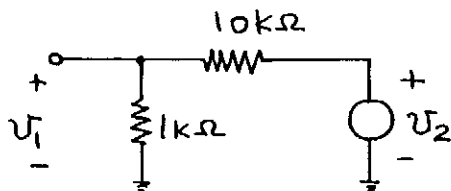
$$R_1 = 1.25k \parallel r_{\pi 3} = 844 \Omega$$

$$R_2 = 6k \parallel 11k = 3.88 \text{ k}\Omega$$

$$\therefore \frac{V_o}{V_i} = \frac{0.53}{26} \frac{1}{1 + \frac{0.53}{26} 54} 844 \frac{3880}{26}$$

$$\therefore a = 1222$$

$$f = h_{12} f = \frac{V_1}{V_2} = \frac{1}{11}$$



$$\therefore \text{loop gain} = \frac{1222}{11} = 111$$

$\therefore$  with feedback gain

$$\frac{V_o}{V_i} = \frac{1222}{1 + 111} = 10.9$$

For the basic amplifier

$$R_{oa} = 11k \parallel 6k = 3.88 \text{ k}\Omega$$

$$r_{ia} = r_{\pi 1} (1 + g_{m1} R_{E1})$$

$$= 9.81 (1 + \frac{0.53}{26} 54) = 20.6 \text{ k}\Omega$$

With feedback

$$R_o = \frac{3880}{112} = 34.6 \Omega$$

$$R_i = 20.6 \times 112 = 2.3 \text{ M}\Omega$$

FEEDBACK AMP

```
VCC 1 0 6V
VEE 2 0 -6V
RL 13 1 25K
Q1 3 5 4 NPN
Q2 1 6 4 NPN
REE 4 2 5K
Q3 7 3 1 PNP
RBIAS 7 2 6K
RF 7 6 10K
RE 6 0 1K
.MODEL NPN NPN BF=200 IS=1E-15
.MODEL PNP PNP BF=100 IS=1E-15
VI 5 0 SIN 0 0.25 10K 0 0
.TRAN 4US 200US
.PLOT TRAN V(7)
.FOUR 10K V(7)
.DC VI -1 1 0.05
.PLOT DC V(7)
.TF V(7) VI
.OPTIONS NOPAGE NOMOD
.WIDTH OUT=80
.OP
.END
```

0\*\*\*\* DC TRANSFER CURVES

VI	V(7)
-5.0D+00	0.0D+00
0.0D+00	5.0D+00
5.0D+00	1.0D+01
1.0D+01	1.5D+01
-6.000D-01	-3.884D+00
-5.500D-01	-3.884D+00
-5.000D-01	-3.884D+00
-4.500D-01	-3.884D+00
-4.000D-01	-3.884D+00
-3.500D-01	-3.818D+00
-3.000D-01	-3.318D+00
-2.500D-01	-2.779D+00
-2.000D-01	-2.234D+00
-1.500D-01	-1.686D+00
-1.000D-01	-1.137D+00
-5.000D-02	-5.862D-01
-4.441D-16	-3.500D-02
5.000D-02	5.167D-01
1.000D-01	1.069D+00
1.500D-01	1.621D+00
2.000D-01	2.173D+00
2.500D-01	2.726D+00
3.000D-01	3.279D+00
3.500D-01	3.831D+00
4.000D-01	4.384D+00
4.500D-01	4.937D+00
5.000D-01	5.490D+00
5.500D-01	5.918D+00
6.000D-01	5.947D+00
6.500D-01	5.950D+00
7.000D-01	5.951D+00
7.500D-01	5.952D+00

8.13-Cont'd

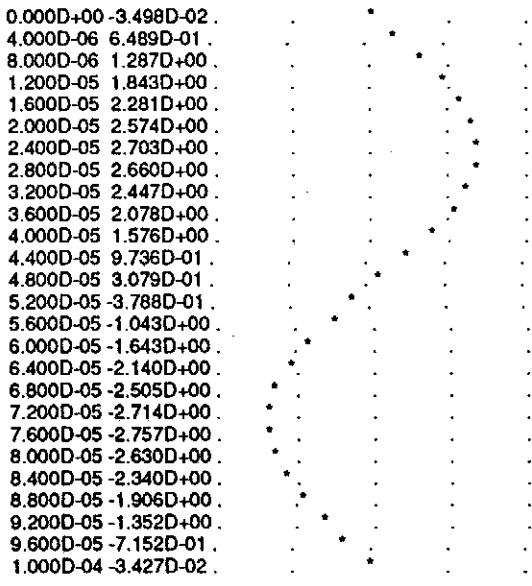
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0**** SMALL SIGNAL BIAS SOLUTION
NODE VOLTAGE
( 1) 6.0000 ( 2) -6.0000 ( 3) 5.2856 ( 4) -0.7006
( 5) -0.0000 ( 6) -0.0053 ( 7) -0.0350

0**** SMALL-SIGNAL CHARACTERISTICS
0 V(7)/VI = 1.103D+01
0 INPUT RESISTANCE AT VI = 2.280D+06
0 OUTPUT RESISTANCE AT V(7) = 3.505D+01

0**** BIPOLAR JUNCTION TRANSISTORS
0 Q1 Q2 Q3
OMODEL NPN NPN PNP
IB 2.91E-06 2.37E-06 -9.91E-06
IC 5.82E-04 4.74E-04 -9.91E-04
VBE 0.701 0.695 -0.714
VBC -5.286 -6.005 5.321
VCE 5.986 6.701 -6.035
BETADC 200.0 200.0 100.0

0**** TRANSIENT ANALYSIS
TIME V(7)
-4.0D+00 -2.0D+00 0.0D+00 2.0D+00 4.0D+00
    
```



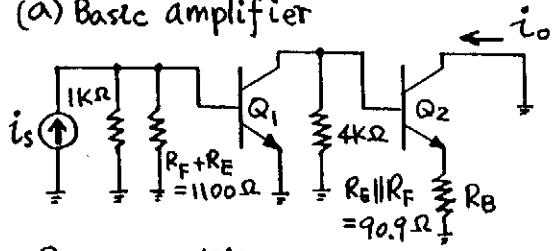
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0**** FOURIER ANALYSIS
FOURIER COMPONENTS OF TRANSIENT RESPONSE V(7)
ODC COMPONENT = -3.085D-02
HARMONIC FREQUENCY FOURIER NORMALIZED PHASE NORM
NO (HZ) COMPONENT COMPONENT (DEG) PHASE (DEG)
1 1.000D+04 2.739D+00 1.000000 -0.004 0.000
2 2.000D+04 4.456D-03 0.001627 -103.114 -103.110
3 3.000D+04 1.392D-03 0.000508 4.977 4.981

TOTAL HARMONIC DISTORTION = 0.170784 PERCENT
    
```

8.17

(a) Basic amplifier



Basic amplifier gain

$$\frac{i_o}{i_s} = -\left(1k \parallel 1.1k \parallel r_{\pi 1}\right) g_{m1} R_1 \frac{g_{m2}}{1 + g_{m2} R_B}$$

$$R_1 = 4k \parallel r_{\pi 2} (1 + g_{m2} R_B) \parallel r_{o1}$$

$$= 4k \parallel 5.2 \left(1 + \frac{90.9}{26}\right) k \parallel 100k$$

$$= 3.30 k\Omega$$

$$\therefore \frac{i_o}{i_s} = -476 \times \frac{3300}{26} \times \frac{1}{26} \times \frac{1}{4.5}$$

$$\therefore a = -516$$

$$r_{ia} = 1k \parallel 1.1k \parallel r_{\pi 1} = 476 \Omega$$

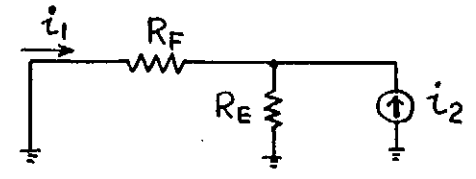
$$r_{oa} = r_{o2} \left(1 + g_{m2} R_B \frac{r_{\pi 2}}{r_{\pi 2} + R_{S2}}\right)$$

$$R_{S2} = r_{o1} \parallel 4k = 3.85 k\Omega$$

$$\therefore r_{oa} = 100 \left(1 + \frac{90.9}{26} \frac{5.2}{5.2 + 3.85}\right) k$$

$$= 300 k\Omega$$

Feedback network



$$f = g_{12f} = \frac{i_1}{i_2} = -\frac{R_E}{R_E + R_F} = -\frac{100}{1100}$$

$$= -\frac{1}{11}$$

$$\therefore \text{loop gain} = \frac{516}{11} = 46.9 = af$$

$\therefore$  with feedback applied

$$\text{overall gain} = \frac{i_o}{i_i} = \frac{a}{1 + af}$$

$$= \frac{-516}{47.9} = -10.8$$

Input resistance

$$R_i = \frac{r_{ia}}{1 + T} = \frac{476}{47.9} = 9.94 \Omega$$

Output resistance

$$R_o = r_{oa} (1 + T) = 300 \times 47.9 = 14.4 M\Omega$$

(b)  $f$  is unchanged

$a$  increases by about 10%

$\therefore$  change in overall gain is

$$\approx \frac{10}{47.9} = 0.2 \%$$

$R_i$  changes by -10% because

$$R_i = \frac{r_{ia}}{1 + af}$$

8.20

(a) Assume high  $\beta$

$$I_{Q8} = \frac{12 - 0.6}{11.4} = 1 \text{ mA}$$

$$\therefore I_{Q7} \approx \frac{1400}{300} \times 1 = 4.7 \text{ mA}$$

$$\therefore I_{Q1} = I_{Q2} = \frac{1}{2} \times 4.7 = 2.3 \text{ mA}$$

$$I_{Q9} = 4.7 \text{ mA}$$

$$\therefore I_{Q3} = I_{Q4} = 2.3 \text{ mA}$$

$$I_{Q10} = I_{Q11} = \frac{1400}{400} \times 1 = 3.5 \text{ mA}$$

$$V_{c3} = V_{c4} = 6 - 1.1 \times 2.3 = 3.5 \text{ V}$$

$\therefore$  DC output voltage

$$= 3.5 - 0.6 = 2.9 \text{ V}$$

Sum currents at collector of  $Q_1$

$$I_{Q1} = \frac{6 - V_{c1}}{2.4} + \frac{2.9 - V_{c1}}{7}$$

$$\therefore 2.3 = 2.5 - 0.42 V_{c1} + 0.41 - 0.14 V_{c1}$$

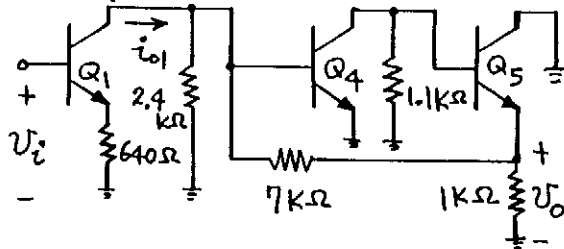
$$\therefore V_{c1} = 1 \text{ V}$$

$\therefore$  Current in  $7 \text{ k}\Omega$  resistor

$$= \frac{2.9 - 1}{7} = 0.27 \text{ mA}$$

$$\therefore I_{Q5} = I_{Q6} = I_{Q10} + 0.27 = 3.8 \text{ mA}$$

(b) Half-circuit



```

733 AMP
VCC 1 0 6V
VEE 2 0 -6V
RC1 1 5 2.4K
RC2 1 6 2.4K
Q1 5 3 7 NPN
Q2 6 4 8 NPN
RE1 7 16 640
RE2 8 16 640
Q3 9 6 15 NPN
Q4 10 5 15 NPN
RC3 1 9 1.1K
RC4 1 10 1.1K
Q5 1 10 11 NPN
Q6 1 9 12 NPN
RF1 11 5 7K
RF2 12 6 7K
RL 11 12 2K
Q7 16 17 18 NPN
Q8 17 17 19 NPN
Q9 15 17 20 NPN
Q10 11 17 13 NPN
Q11 12 17 14 NPN
RQ7 18 2 300
RQ8 19 2 1.4K
RQ9 20 2 300
RQ10 13 2 400
RQ11 14 2 400
RBIAS 1 17 10K
.MODEL NPN NPN BF=100 IS=1E-13
V11 3 0 0V
V12 4 0 0V
.TF V(11,12) V11
.OPTIONS NOPAGE NOMOD
.WIDTH OUT=80
.OP
.END
    
```

0\*\*\*\* SMALL SIGNAL BIAS SOLUTION

NODE VOLTAGE			
(1)	6.0000	(2)	-6.0000
(3)	-0.0000	(4)	-0.0000
(5)	1.7678	(6)	1.7678
(7)	-0.6128	(8)	-0.6128
(9)	3.8225	(10)	3.8225
(11)	3.1973	(12)	3.1973
(13)	-4.8003	(14)	-4.8003
(15)	1.1550	(16)	-1.8721
(17)	-4.1766	(18)	-4.8076
(19)	-4.7686	(20)	-4.8076

0\*\*\*\* BIPOLAR JUNCTION TRANSISTORS

Q	Q1	Q2	Q3	Q4	Q5	Q6	Q7
0	MODEL	NPN	NPN	NPN	NPN	NPN	NPN
IB	1.95E-05	1.95E-05	1.95E-05	1.95E-05	3.14E-05	3.14E-05	3.94E-05
IC	1.95E-03	1.95E-03	1.95E-03	1.95E-03	3.14E-03	3.14E-03	3.94E-03
VBE	0.613	0.613	0.613	0.613	0.625	0.625	0.631
VBC	-1.768	-1.768	-2.055	-2.055	-2.178	-2.178	-2.305
VCE	2.381	2.381	2.667	2.667	2.803	2.803	2.936
BETADC	100.00	100.00	100.00	100.00	100.00	100.00	100.00
GM	7.53E-02	7.53E-02	7.53E-02	7.53E-02	1.22E-01	1.22E-01	1.52E-01
RPI	1.33E+03	1.33E+03	1.33E+03	1.33E+03	8.23E+02	8.23E+02	6.57E+02
RO	9.46E+11	9.46E+11	9.54E+11	9.54E+11	9.56E+11	9.56E+11	9.58E+11

Q8	Q9	Q10	Q11
0	MODEL	NPN	NPN
IB	8.71E-06	3.94E-05	2.97E-05
IC	8.71E-04	3.94E-03	2.97E-03
VBE	0.592	0.631	0.624
VBC	0.000	-5.332	-7.374
VCE	0.592	5.963	7.998
BETADC	100.000	100.000	100.000
GM	3.37E-02	1.52E-01	1.15E-01
RPI	2.97E+03	6.57E+02	8.71E+02
RO	2.05E+11	9.82E+11	9.87E+11

\*\*\*\*\*  
HAND ANALYSIS STARTS WITH BIAS STRING: Q8 AND RESISTORS OF 10K AND 1.4K AND FINDS  $I_{C8} = 1 \text{ mA}$ . BUT IT FAILS TO ACCOUNT FOR BASE CURRENTS OF Q7, Q9, Q10, Q11.

USING SPICE, WE SEE THAT THIS 1MA IS DIVIDED AMONG THESE TRANSISTORS:  $1 \text{ mA} = I_{C8} + I_{B7} + I_{B9} + I_{B10} + I_{B11}$

SO THE SPICE DC BIAS CURRENTS OF TRANSISTORS ARE DIFFERENT FROM THE VALUES OBTAINED BY HAND.

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**** SMALL-SIGNAL CHARACTERISTICS
V(11,12)/V11 = 9.531D+00
INPUT RESISTANCE AT V11 = 1.319D+05
OUTPUT RESISTANCE AT V(11,12) = 3.793D+00
    
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$$R_i = r_{\pi 1} + (1 + \beta) R_{E1}$$

$$= \frac{100 \times 26}{2.3} + 101 \times 640 = 66 \text{ k}\Omega$$

— for the half circuit

$$\therefore R_i = 132 \text{ k}\Omega \text{ — for the complete circuit}$$

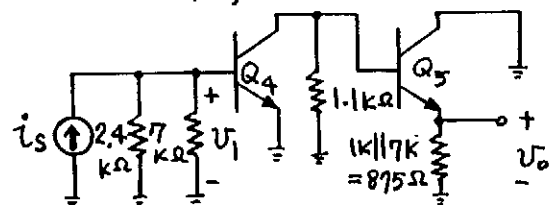
For the first stage

$$\frac{i_{o1}}{v_i} = -\frac{1}{640} \frac{1}{1 + \frac{1}{\beta} \left( \frac{26}{2.3} + 640 \right)}$$

$$= -1.52 \text{ mA/V}$$

Consider the shunt-shunt feedback stage.

Basic amplifier is



8.20-Cont'd

$$V_i = i_s(2.4k \parallel 7k \parallel r_{\pi 4})$$

$$= i_s \times 0.69k$$

$$R_{i5} = r_{\pi 5} + (1 + \beta) \times 875$$

$$= 684 + 88.4k = 89k \Omega$$

$$\therefore \frac{v_o}{i_s} = -0.69k \times g_{m4} [1.1k \parallel 89k]$$

$$= -0.69k \times \frac{2.3}{26} \times 1087$$

$$\therefore a = -66.3 k\Omega$$

$$f = -\frac{1}{7k}$$

\(\therefore\) For the output stage with feedback applied

$$\frac{v_o}{i_{o1}} = \frac{a}{1 + af} = \frac{-281k}{1 + 9.47} = -6.33 k\Omega$$

\(\therefore\) for the overall circuit

$$\frac{v_o}{v_i} = 1.52 \times 10^{-3} \times 6.33 \times 10^3 = 9.6$$

Loop gain of output stage

$$T = af = 9.47$$

Output impedance of half circuit

$$= 875 \parallel \left[ \frac{1}{g_{m5}} + \frac{1100}{\beta} \right]$$

$$= 875 \parallel [7 + 11] = 18 \Omega$$

\(\therefore\) For the complete circuit

$$V_{oa} = 36 \Omega, \text{ and with feedback applied, } R_o = \frac{36}{1 + T} = 3.6 \Omega$$

8.23

$$\frac{V_{DD} - V_{GS2}}{10k} = I_{D2} = \frac{30\mu}{2} 20(V_{GS2} - 0.8)^2$$

$$5 - a = 3(a - 0.8)^2$$

$$= 3a^2 - 4.8a + 1.92$$

$$0 = 3a^2 - 3.8a - 3.08$$

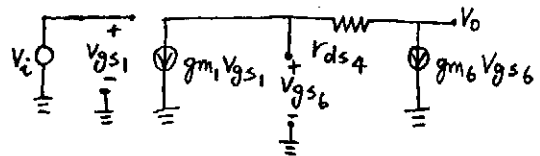
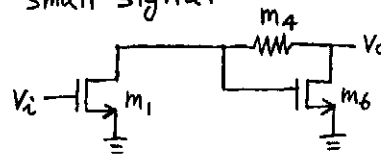
$$a = \frac{+3.8 \pm \sqrt{3.8^2 - 4(3)(-3.08)}}{6}$$

$$V_{GS2} = 1.83V$$

$$I_{D2} = \frac{30\mu}{2} 20(1.83 - 0.8)^2$$

$$= 317 \mu A = I_{D1} = I_{D5} = I_{D6}$$

small signal



$$V_o = V_{gs6} - g_{m6} V_{gs6} r_{ds4}$$

$$g_{m1} = g_{m6}$$

$$-g_{m1} V_{gs1} = g_{m6} V_{gs6}$$

$$-V_{gs1} = V_{gs6} = -V_i$$

$$V_o = -V_i + g_{m6} V_i r_{ds4}$$

$$\frac{V_o}{V_i} = -1 + g_{m6} r_{ds4}$$

$$g_{m6} = \sqrt{2(317\mu)(60\mu)(20)}$$

$$= 872 \mu A/V$$

$$g_{ds4} = \mu_n C_{ox} \frac{W}{L} (V_{GS4} - V_{t4})$$

$$= 150\mu (V_c - 1.53 - 1.14)$$

$$= 150\mu (V_c - 2.67)$$

$$V_{t4} = V_{t0} + \gamma(\sqrt{V_{SB4} + 2\phi_f} - \sqrt{2\phi_f})$$

$$= 0.8 + 0.5(\sqrt{1.53 + 0.6} - \sqrt{0.6})$$

$$= 1.14V$$

$$V_{SB4} = V_{GS6} = V_{t6} + \sqrt{\frac{2I_{D6}}{\mu C_{ox} \frac{W}{L}_6}}$$

$$= 0.8 + \sqrt{\frac{2(317\mu)}{60\mu(20)}}$$

$$= 1.53V$$

$$V_c = 3V$$

$$g_{ds4} = 150\mu(3 - 2.67)$$

$$= 49.5\mu$$

$$r_{ds4} = 20.2k$$

$$\frac{V_o}{V_i} = -1 + (872\mu)(20.2k) = 16.6$$

8.23-Cont'd

$$V_c = 4V$$

$$g_{ds4} = 150\mu(4 - 2.67)$$

$$= 200\mu$$

$$r_{ds4} = 5.01k$$

$$\frac{V_o}{V_i} = -1 + (872\mu)(5.01k)$$

$$= 3.37$$

$$R_o = \frac{1}{g_{m6}} = \frac{1}{872\mu} = 1.15k\Omega$$

8.24

$$I_{D1} = I_{D2} = \frac{1}{2} I_{D6} = 100\mu A = I_{D3}$$

$$I_{D8} = 200\mu A$$

$$a = \frac{1}{2} g_{m1} (2r_{o2} || r_{o3}) \frac{g_{m8}(21k)}{1 + g_{m8}(21k)}$$

$$= \frac{1}{2} (693\mu)(222k)(0.954)$$

$$= 73.4$$

$$g_{m1} = \sqrt{2(100\mu)(60\mu)40}$$

$$= 693\mu A/V$$

$$r_{o2} = r_{o3} = \frac{1}{\lambda I_D} = \frac{1}{0.03(100\mu)}$$

$$= 333k$$

$$g_{m8} = \sqrt{2(200\mu)(60\mu)40}$$

$$= 980\mu A/V$$

$$f = \frac{1k}{1k + 20k} = \frac{1}{21}$$

$$T = af = 3.5$$

$$A = \frac{a}{1+T} = \frac{73.4}{4.5} = 16.3 = \frac{V_o}{V_i}$$

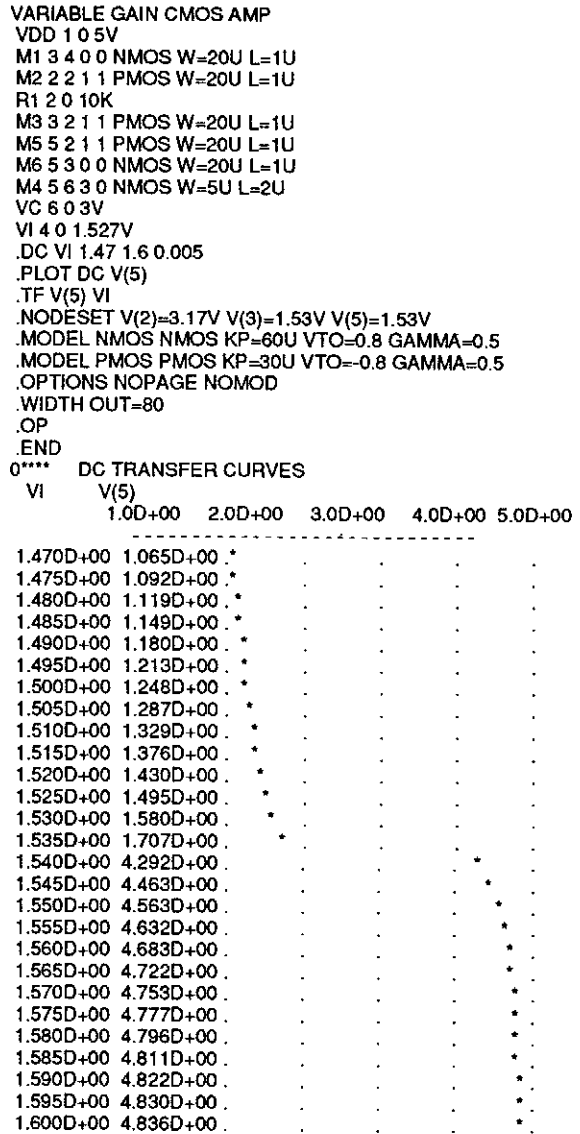
$$R_o = \frac{r_{out}}{1+T} = \frac{973}{4.5}$$

$$= 216\Omega$$

$$r_{out} = 21k || \frac{1}{g_{m8}}$$

$$= 21k || 1.02k$$

$$= 973\Omega$$



0\*\*\*\* SMALL SIGNAL BIAS SOLUTION

NODE	VOLTAGE
( 1 )	5.0000 ( 2 ) 3.1718 ( 3 ) 1.5271 ( 4 ) 1.5270
( 5 )	1.5259 ( 6 ) 3.0000

0\*\*\*\* MOSFETS

	M1	M2	M3	M5	M6	M4
0MODEL	NMOS	PMOS	PMOS	PMOS	NMOS	NMOS
ID	3.17E-04	-3.17E-04	-3.17E-04	-3.17E-04	3.17E-04	-5.96E-08
VGS	1.527	-1.828	-1.828	-1.828	1.527	1.473
VDS	1.527	-1.828	-3.473	-3.474	1.526	-0.001
VBS	0.000	0.000	0.000	0.000	0.000	-1.527
VTH	0.800	-0.800	-0.800	-0.800	0.800	1.142
VDSAT	0.727	-1.028	-1.028	-1.028	0.727	0.332
GM	8.72E-04	6.17E-04	6.17E-04	6.17E-04	8.73E-04	1.80E-07
GDS	0.00E+0	0.00E+0	0.00E+0	0.00E+0	0.00E+0	4.97E-05
GMB	2.82E-04	1.99E-04	1.99E-04	1.99E-04	2.82E-04	3.08E-08

0\*\*\*\* SMALL-SIGNAL CHARACTERISTICS

0	V(5)/VI	= 1.649D+01
0	INPUT RESISTANCE AT VI	= 1.000D+20
0	OUTPUT RESISTANCE AT V(5)	= 1.141D+03

B.24-Cont'd

VARIABLE GAIN CMOS AMP

```
VDD 1 0 5V
M1 3 4 0 0 NMOS W=20U L=1U
M2 2 2 1 1 PMOS W=20U L=1U
R1 2 0 10K
M3 3 2 1 1 PMOS W=20U L=1U
M5 5 2 1 1 PMOS W=20U L=1U
M6 5 3 0 0 NMOS W=20U L=1U
M4 5 6 3 0 NMOS W=5U L=2U
VC 6 0 4V
VI 4 0 1.527V
.DC VI 1.0 1.8 0.05
.PLOT DC V(5)
.TF V(5) VI
.NODESET V(2)=3.17V V(3)=1.53V V(5)=1.53V
.MODEL NMOS NMOS KP=60U VTO=0.8 GAMMA=0.5
.MODEL PMOS PMOS KP=30U VTO=-0.8 GAMMA=0.5
.OPTIONS NOPAGE NOMOD
.WIDTH OUT=80
.OP
.END
```

0\*\*\*\* DC TRANSFER CURVES

VI	V(5)	0.0D+00	2.0D+00	4.0D+00	6.0D+00	8.0D+00
1.000D+00	7.255D-01	*	.	.	.	.
1.050D+00	7.496D-01	*	.	.	.	.
1.100D+00	7.806D-01	*	.	.	.	.
1.150D+00	8.197D-01	*	.	.	.	.
1.200D+00	8.687D-01	*	.	.	.	.
1.250D+00	9.299D-01	*	.	.	.	.
1.300D+00	1.003D+00	*	.	.	.	.
1.350D+00	1.089D+00	*	.	.	.	.
1.400D+00	1.188D+00	*	.	.	.	.
1.450D+00	1.303D+00	*	.	.	.	.
1.500D+00	1.441D+00	*	.	.	.	.
1.550D+00	1.607D+00	*	.	.	.	.
1.600D+00	1.803D+00	*	.	.	.	.
1.650D+00	2.038D+00	*	.	.	.	.
1.700D+00	2.339D+00	*	.	.	.	.
1.750D+00	4.054D+00	*	.	.	.	.
1.800D+00	4.132D+00	*	.	.	.	.

0\*\*\*\* SMALL SIGNAL BIAS SOLUTION

NODE VOLTAGE  
 ( 1) 5.0000 ( 2) 3.1718 ( 3) 1.5271 ( 4) 1.5270  
 ( 5) 1.5268 ( 6) 4.0000

0\*\*\*\* MOSFETS

0	M1	M2	M3	M5	M6	M4
0MODEL	NMOS	PMOS	PMOS	PMOS	NMOS	NMOS
ID	3.17E-04	-3.17E-04	-3.17E-04	-3.17E-04	3.17E-04	-5.96E-08
VGS	1.527	-1.828	-1.828	-1.828	1.527	2.473
VDS	1.527	-1.828	-3.473	-3.473	1.527	0.000
VBS	0.000	0.000	0.000	0.000	0.000	-1.527
VTH	0.800	-0.800	-0.800	-0.800	0.800	1.142
VDSAT	0.727	-1.028	-1.028	-1.028	0.727	1.331
GM	8.72E-04	6.17E-04	6.17E-04	6.17E-04	8.73E-04	4.48E-08
GDS	0.00E+0	0.00E+0	0.00E+0	0.00E+0	0.00E+0	2.00E-04
GMB	2.82E-04	1.99E-04	1.99E-04	1.99E-04	2.82E-04	7.68E-09

0\*\*\*\* SMALL-SIGNAL CHARACTERISTICS

0 V(5)/VI = 3.369D+00  
 0 INPUT RESISTANCE AT VI = 1.000D+20  
 0 OUTPUT RESISTANCE AT V(5) = 1.146D+03

CMOS FEEDBACK AMP

```
VDD 1 0 5V
VSS 9 0 -5V
M4 2 2 1 1 PMOS W=20U L=1U
I1 2 3 100UA
M5 3 3 9 9 NMOS W=20U L=1U
M6 6 3 9 9 NMOS W=40U L=1U
M1 1 4 6 9 NMOS W=40U L=1U
M2 5 7 6 9 NMOS W=40U L=1U
M3 5 2 1 1 PMOS W=20U L=1U
M8 1 5 8 9 NMOS W=40U L=1U
M7 8 3 9 9 NMOS W=40U L=1U
RF 8 7 20K
RE 7 0 1K
VI 4 0 0V
.TF V(8) VI
.MODEL NMOS NMOS KP=60U VTO=0.8 LAMBDA=0.03
.MODEL PMOS PMOS KP=30U VTO=-0.8 LAMBDA=0.03
.OPTIONS NOPAGE NOMOD
.WIDTH OUT=80
.OP
.END
```

0\*\*\*\* SMALL SIGNAL BIAS SOLUTION

NODE VOLTAGE  
 ( 1) 5.0000 ( 2) 3.6341 ( 3) -3.7989 ( 4) -0.0000  
 ( 5) 1.4134 ( 6) -1.0776 ( 7) 0.0096 ( 8) 0.2016  
 ( 9) -5.0000

0\*\*\*\* MOSFETS

0	M4	M5	M6	M1	M2	M3	M8
0MODEL	PMOS	NMOS	NMOS	NMOS	NMOS	PMOS	NMOS
ID	-1.00E-04	1.00E-04	2.16E-04	1.09E-04	1.06E-04	-1.06E-04	2.33E-04
VGS	-1.366	1.201	1.201	1.078	1.087	-1.366	1.212
VDS	-1.366	1.201	3.922	6.078	2.491	-3.587	4.798
VBS	0.000	0.000	0.000	-3.922	-3.922	0.000	-5.202
VTH	-0.800	0.800	0.800	0.800	0.800	-0.800	0.800
VDSAT	-0.566	0.401	0.401	0.278	0.287	-0.566	0.412
GM	3.54E-04	4.99E-04	1.08E-03	7.88E-04	7.41E-04	3.76E-04	1.13E-03
GDS	2.88E-06	2.90E-06	5.79E-06	2.77E-06	2.97E-06	2.88E-06	6.10E-06

0\*\*\*\* M7

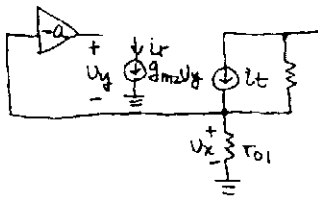
0MODEL	NMOS
ID	2.23E-04
VGS	1.201
VDS	5.202
VBS	0.000
VTH	0.800
VDSAT	0.401
GM	1.11E-03
GDS	5.79E-06

0\*\*\*\* SMALL-SIGNAL CHARACTERISTICS

0 V(8)/VI = 1.662D+01  
 0 INPUT RESISTANCE AT VI = 1.000D+20  
 0 OUTPUT RESISTANCE AT V(8) = 1.707D+02

8.26

(a)  $g_{m2}$  is the controlled source.



$$R_{out}(g_{m2}=0) = r_{o1} + r_{o2}$$

$$R(\text{short}) = (r_{o1} \parallel r_{o2})(a+1)g_{m2}$$

$$R(\text{open}) = 0$$

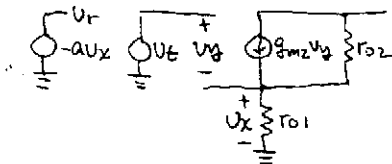
$$R_{out} = R_{out}(g_{m2}=0) \frac{1+R(\text{short})}{1+R(\text{open})}$$

$$= (r_{o1} + r_{o2}) \frac{1+(r_{o1} \parallel r_{o2})(a+1)g_{m2}}{1+0}$$

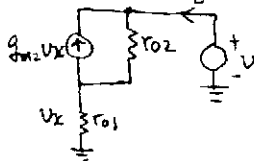
$$= r_{o1} + r_{o2} + (a+1)g_{m2}r_{o1}r_{o2}$$

$$\approx a g_{m2} r_{o1} r_{o2}$$

(b)  $a$  is the controlled source.



$a=0$



$$\frac{v_x}{r_{o1}} = g_{m2} v_x + \frac{v_x - v}{r_{o2}}$$

$$R_{out}(a=0) = \frac{v}{i} = \frac{v}{v_x/r_{o1}}$$

$$= g_{m2} r_{o1} r_{o2} + r_{o1} - r_{o2}$$

$$\approx g_{m2} r_{o1} r_{o2}$$

The output is short

$$v_x = g_{m2}(v_t - v_x)(r_{o1} \parallel r_{o2})$$

$$v_x = \frac{g_{m2}(r_{o1} \parallel r_{o2})}{1 + g_{m2}(r_{o1} \parallel r_{o2})} v_t$$

$$R(\text{short}) = a \frac{g_{m2}(r_{o1} \parallel r_{o2})}{1 + g_{m2}(r_{o1} \parallel r_{o2})}$$

$R(\text{open}) = 0$  ( $v_x = 0$  when the output is open)

$$R_{out} = R_{out}(a=0) \frac{1+R(\text{short})}{1+R(\text{open})}$$

$$\approx g_{m2} r_{o1} r_{o2} \frac{1 + \frac{g_{m2}(r_{o1} \parallel r_{o2})}{1 + g_{m2}(r_{o1} \parallel r_{o2})}}{1+0}$$

$$\approx a g_{m2} r_{o1} r_{o2}$$

(c) The results are the same, as they should be, even though the terms  $R_{out}(k=0)$ ,  $R(\text{open})$ , and  $R(\text{short})$  differ in (a) and (b).