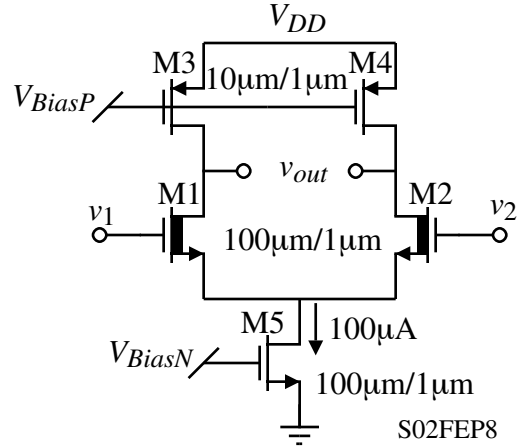


## Homework Assignment No. 13 - Solutions

### Problem 1 - (10 points)

A differential CMOS amplifier using depletion mode input devices is shown. Assume that the normal MOSFETs parameters are  $K_N' = 110\text{V}/\mu\text{A}^2$ ,  $V_{TN} = 0.7\text{V}$ ,  $\lambda_N = 0.04\text{V}^{-1}$  and for the PMOS transistors are  $K_P' = 110\text{V}/\mu\text{A}^2$ ,  $V_{TP} = 0.7\text{V}$ ,  $\lambda_P = 0.04\text{V}^{-1}$ . For the depletion mode NMOS transistors, the parameters are the same as the normal NMOS except that  $V_{TN} = -0.5\text{V}$ . (a.) What is the maximum input common-mode voltage,  $V_{icm}^+(\text{max})$ ? (b.) What is the minimum input common-mode voltage,  $V_{icm}^-(\text{min})$ ? (c.) What value of  $V_{DD}$  gives an  $ICMR = 0.5V_{DD}$ ?



### Solution

$$(a.) \quad V_{icm}^+(\text{max}) = V_{DD} - V_{SD3}(\text{sat}) - V_{DS1}(\text{sat}) + V_{GS1}(50\mu\text{A})$$

$$i_D = \frac{\beta}{2} (V_{GS1} - V_{T1})^2 \rightarrow V_{GS1} = \sqrt{\frac{2i_D}{\beta}} + V_{T1} = V_{DS1}(\text{sat}) + V_{T1}$$

$$\therefore V_{icm}^+(\text{max}) = V_{DD} - V_{SD3}(\text{sat}) + V_{T1} = V_{DD} - \sqrt{\frac{2I_{D3}}{\beta_3}} + V_{T1}$$

$$V_{icm}^+(\text{max}) = V_{DD} - 0.4472 - 0.5 = \underline{\underline{V_{DD} - 0.9472}}$$

$$(b.) \quad V_{icm}^-(\text{min}) = V_{DS5}(\text{sat}) + V_{GS1}(50\mu\text{A}) = V_{DS5}(\text{sat}) + V_{DS1}(\text{sat}) + V_{T1}$$

$$V_{icm}^-(\text{min}) = \sqrt{\frac{2I_{D5}}{\beta_5}} + \sqrt{\frac{2I_{D1}}{\beta_1}} + V_{T1} = 0.1348 + 0.0953 - 0.5 = \underline{\underline{-0.2698\text{V}}}$$

$$(c.) \quad ICMR = V_{icm}^+(\text{max}) - V_{icm}^-(\text{min}) = V_{DD} - 0.9472 + 0.2698 = V_{DD} - 0.6774$$

$$\therefore V_{DD} - 0.6774 = 0.5V_{DD} \rightarrow V_{DD} = 2(0.6774) = \underline{\underline{1.355\text{V}}}$$

Problem 2 – (10 points)

If the poles of a two-stage comparator are both equal to  $-10^7$  radians/sec., find the maximum slope and the time it occurs if the magnitude of the input step is  $10V_{in(min)}$  and  $V_{OH} - V_{OL} = 1V$ . What must be the  $SR$  of this comparator to avoid slewing?

Solution

The response to a step response to the above comparator can be written as,

$$v_{out}' = 1 - e^{-t_n} - t_n e^{-t_n} \quad \text{where } v_{out}' = \frac{v_{out}}{A_v(0)V_{in}} \text{ and } t_n = tp_1$$

To find the maximum slope, differentiate twice and set to zero.

$$\frac{dv_{out}'}{dt_n} = e^{-t_n} + t_n e^{-t_n} - e^{-t_n} = t_n e^{-t_n}$$

$$\frac{d^2 v_{out}'}{dt_n^2} = -t_n e^{-t_n} + e^{-t_n} = 0 \quad \Rightarrow \quad (1 - t_n)e^{-t_n} = 0 \quad \Rightarrow \quad t_n(\max) = tp_1 = 1$$

$$\therefore t_n(\max) = 1 \text{ sec} \quad \text{and } t(\max) = \frac{t_n}{|p_1|} = \frac{1}{10^7} = \underline{0.1 \mu\text{s}}$$

$$\frac{dv_{out}'(\max)}{dt_n} = e^{-1} = 0.3679 \text{ V/sec} \quad \text{or} \quad \frac{dv_{out}'(\max)}{dt_n} = 3.679 \text{ V}/\mu\text{s}$$

$$\frac{dv_{out}'(\max)}{dt} = 10(V_{OH} - V_{OL}) \cdot \frac{dv_{out}'(\max)}{dt_n} = \underline{36.79 \text{ V}/\mu\text{s}}$$

$\therefore$  Therefore, the slew rate of the comparator should be greater than  $36.79 \text{ V}/\mu\text{s}$  to avoid slewing.

Problem 3 – (10 points)

Repeat Ex. 8.2-5 with  $v_{G2}$  constant and the waveform of Fig. 8.2-6 applied to  $v_{G1}$ .

Solution

Output fall time,  $t_r$ :

The initial states are  $v_{o1} \approx -2.5V$  and  $v_{out} \approx 2.5V$ . The reasoning for  $v_{o1}$  is interesting and should be understood. When  $V_{G1} = -2.5V$  and  $V_{G2} = 0V$ , the current in M1 is zero. This means the current is also zero in M4. Therefore,  $v_{o1}$  goes very negative and as M2 acts like a switch with  $V_{DS} \approx 0$ . Since the only current for M3 comes through M2 and from  $C_I$ , the voltage across M3 eventually collapses and  $I_3$  becomes zero which causes  $v_{o1} \approx -2.5V$ .

From Example 8.2-5, the trip point of the second stage is 1.465V, therefore the rise time of the first stage is,

$$t_{r1} = 0.2\text{pF} \left( \frac{1.465 + 2.5}{30\mu\text{A}} \right) = 26.4\text{ns}$$

The fall time of the second stage is found in Example 8.2-5 and is  $t_{f2} = 53.4\text{ns}$ . The total output fall time is

$$\therefore t_r = t_{r1} + t_{f2} = \underline{79.8\text{ns}}$$

Output rise time,  $t_r$ :

The initial states for this analysis are  $v_{o1} \approx 2.5V$  and  $v_{out} \approx -2.5V$ .

The input stage fall time is,

$$t_{f1} = 0.2\text{pF} \left( \frac{2.5 - 1.465}{30\mu\text{A}} \right) = 6.9\text{ns}$$

The output stage rise time is found by determining the best guess for  $V_{G6}$ . Since  $V_{G6}$  is going from 1.465 to  $-2.5V$ , let us approximate  $V_{G6}$  as

$$V_{G6} \approx 0.5(1.465 - 2.5) = -0.5175 \quad \Rightarrow \quad V_{SG6} = 2.5 - (-0.5175) = 3.0175V$$

$$\therefore I_6 = \frac{1}{2}K_P \left( \frac{W_6}{L_6} \right) (V_{SG6} - |V_{TP}|)^2 = 0.5 \cdot 50 \times 10^{-6} \cdot 38 (3.0175 - 0.7)^2 = 5102\mu\text{A}$$

$$t_{r2} = 5\text{pF} \left( \frac{2.5}{5102\mu\text{A} - 234\mu\text{A}} \right) = 2.6\text{ns}$$

The total output rise time is,

$$\therefore t_r = t_{f1} + t_{r2} = \underline{9.5\text{ns}}$$

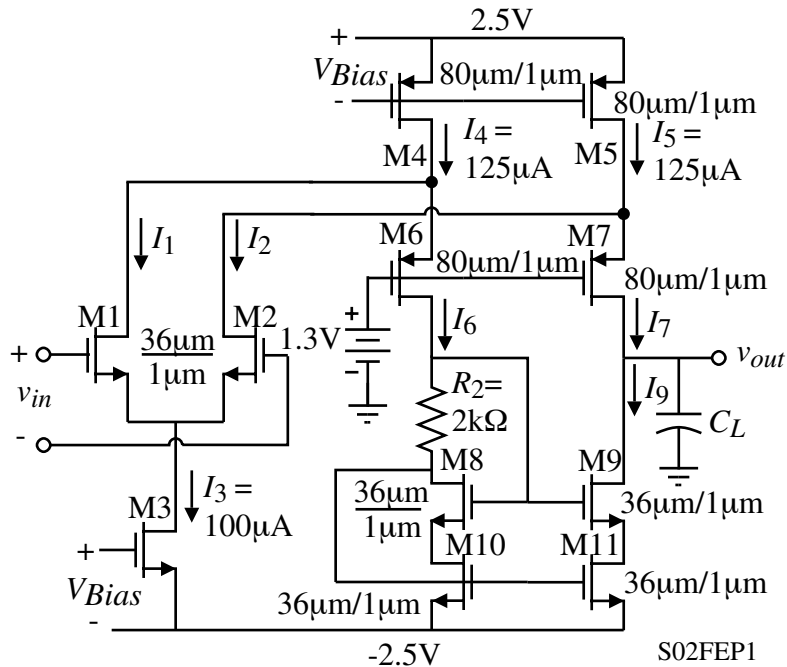
The propagation time delay of the comparator is,

$$t_p = t_r + t_r = \underline{44.7\text{ns}}$$



Problem 5

If the folded-cascode op amp shown having a small-signal voltage gain of  $7464\text{V/V}$  is used as a comparator, find the dominant pole if  $C_L = 5\text{pF}$ . If the input step is  $10\text{mV}$ , determine whether the response is linear or slewing and find the propagation delay time. Assume the parameters of the NMOS transistors are  $K_N' = 110\text{V}/\mu\text{A}^2$ ,  $V_{TN} = 0.7\text{V}$ ,  $\lambda_N = 0.04\text{V}^{-1}$  and for the PMOS transistors are  $K_P' = 50\text{V}/\mu\text{A}^2$ ,  $V_{TP} = -0.7\text{V}$ ,  $\lambda_P = 0.05\text{V}^{-1}$ .

Solution

$V_{OH}$  and  $V_{OL}$  can be found from many approaches. The easiest is simply to assume that  $V_{OH}$  and  $V_{OL}$  are  $2.5\text{V}$  and  $-2.5\text{V}$ , respectively. However, no matter what the input, the values of  $V_{OH}$  and  $V_{OL}$  will be in the following range,

$$(V_{DD} - 2V_{ON}) < V_{OH} < V_{DD} \quad \text{and} \quad V_{DD} < V_{OH} < (V_{SS} + 2V_{ON})$$

The reasoning is as follows, suppose  $V_{in} > 0$ . This gives  $I_1 > I_2$  which gives  $I_6 < I_7$  which gives  $I_9 < I_7$ .  $V_{out}$  will increase until  $I_7$  equals  $I_9$ . The only way this can happen is for M5 and M7 to leave saturation. The same reasoning holds for  $V_{in} < 0$ .

Therefore assuming that  $V_{OH}$  and  $V_{OL}$  are  $2.5\text{V}$  and  $-2.5\text{V}$ , respectively, we get

$$V_{in}(\text{min}) = \frac{5\text{V}}{7464} = 0.67\text{mV} \quad \rightarrow \quad k = \frac{10\text{mV}}{0.67\text{mV}} = 14.93$$

Problem 5 – Continued

The folded-cascode op amp as a comparator can be modeled by a single dominant pole. This pole is found as,

$$p_1 = \frac{1}{R_{out}C_L} \text{ where } R_{out} \approx g_{m9}r_{ds9}r_{ds11} \parallel [g_{m7}r_{ds7}(r_{ds2} \parallel r_{ds5})]$$

$$g_{m9} = \sqrt{2 \cdot 75 \cdot 110 \cdot 36} = 771 \mu\text{S}, \quad g_{ds9} = g_{ds11} = 75 \times 10^{-6} \cdot 0.04 = 3 \mu\text{S}, \quad g_{ds2} = 50 \times 10^{-6} (0.04) = 2 \mu\text{S}$$

$$g_{m7} = \sqrt{2 \cdot 75 \cdot 50 \cdot 80} = 775 \mu\text{S}, \quad g_{ds5} = 125 \times 10^{-6} \cdot 0.05 = 6.25 \mu\text{S}, \quad g_{ds7} = 50 \times 10^{-6} (0.05) = 3.75 \mu\text{S}$$

$$g_{m9}r_{ds9}r_{ds11} = (771 \mu\text{S}) \left( \frac{1}{3 \mu\text{S}} \right) \left( \frac{1}{3 \mu\text{S}} \right) = 85.67 \text{M}\Omega$$

$$g_{m7}r_{ds7}(r_{ds2} \parallel r_{ds5}) \approx (775 \mu\text{S}) \left( \frac{1}{3.75 \mu\text{S}} \right) \left( \frac{1}{2 \mu\text{S}} \parallel \frac{1}{6.25 \mu\text{S}} \right) = 25.05 \text{M}\Omega,$$

$$R_{out} \approx 85.67 \text{M}\Omega \parallel 25.05 \text{M}\Omega = 19.4 \text{M}\Omega$$

The dominant pole is found as,  $p_1 = \frac{1}{R_{out}C_L} = \frac{1}{19.4 \times 10^6 \text{pF}} = 10,318 \text{ rps}$

The time constant is  $\tau_1 = 96.9 \mu\text{s}$ .

For a dominant pole system, the step response is,  $v_{out}(t) = A_{vd}(1 - e^{-t/\tau_1})V_{in}$

The slope is the largest at  $t = 0$ . Evaluating this slope gives,

$$\frac{dv_{out}}{dt} = \frac{A_{vd}}{\tau_1} e^{-t/\tau_1} V_{in} \text{ For } t = 0, \text{ the slope is } \frac{A_{vd}}{\tau_1} V_{in} = \frac{7464}{96.9 \mu\text{s}} (10 \text{mV}) = 0.77 \text{V}/\mu\text{s}$$

The slew rate of this op amp/comparator is  $SR = \frac{I_3}{C_L} = \frac{100 \mu\text{A}}{5 \text{pF}} = 20 \text{V}/\mu\text{s}$

Therefore, the comparator does not slew and its propagation delay time is found from the linear response as,

$$t_P = \tau_1 \ln\left(\frac{2k}{2k-1}\right) = 96.9 \mu\text{s} \cdot \ln\left(\frac{2 \cdot 14.93}{2 \cdot 14.93 - 1}\right) = (96.9 \mu\text{s})(0.0341) = \underline{\underline{3.3 \mu\text{s}}}$$